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AN INVERSE ANALYSIS OF
ELECTROTHERMAL-CHEMICAL (ETC) GUN
EXPERIMENTAL DATA

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<p>An inverse analysis is presented as one method of assessing ballistic control exhibited in electrothermal-chemical (ETC) experimental gun firings. The analysis attempts to determine the decomposition or gas generation rate necessary to satisfy an energy balance equation as gleaned from available experimental data. The apparent functional relationship between the electrical energy input and working fluid mass consumed is examined. As applied in this report, the inverse analysis of ETC gun firing data is essentially an energy balance between projectile kinetic energy, gas kinetic energy, and gas internal energy. Lagrange assumptions are made for the pressure gradient and gas velocity. Thermochemistry is assumed to be variable depending on the plasma energy to working fluid mass ratio. A sample database consisting of 20-mm and 30-mm gun firings is examined.</p>						
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1. INTRODUCTION

The electrothermal-chemical (ETC) gun, generically shown in Figure 1, is a propulsion concept which utilizes a low mass, high energy plasma to initiate and, hopefully, control the combustion/vaporization of the working fluid (propellant) during the ballistic cycle. Controlling combustion (exothermic working fluid) or vaporization (endothermic working fluid) of the working fluid in the ETC gun is necessary in order to tailor the pressure-time profile in the gun. Theoretically, tailoring the pressure-time profile to obtain a "flatter" and extended pressure curve should result in enhanced performance (increased muzzle energy) and provide a "softer" launch environment to enhance projectile integrity, especially for "smart" projectiles. In addition, precise control of the pressure history should also allow for the required projectile velocity repeatability required of indirect fire support (artillery) applications.

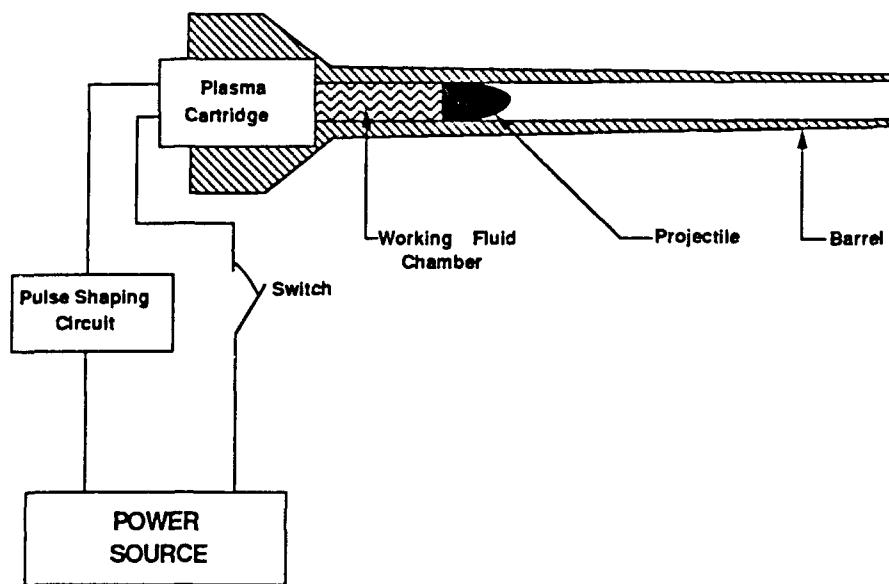


Figure 1. Schematic of ETC Gun.

One method of assessing the control exerted by the plasma on the combustion/ vaporization process is through the use of an inverse analysis which computes the decomposition or gas generation rate of the working fluid given experimental measurements of pressure, projectile motion, and plasma energy histories as an input to the model. If the plasma is controlling the process, then the inverse analysis should show decomposition rates to be a "strong" function of the plasma input (plasma energy-time input).

To illustrate the method, an inverse analysis of 20-mm and 30-mm ETC firings using an exothermic working fluid is presented. The objective is to ascertain to what extent these experimental ETC firings indicate control of the working fluid combustion by the plasma energy input to the gun. The results of the inverse analysis for these data sets are viewed as qualitative since the experimental measurements are not precise; for example, the projectile position is not accurately known from the experimental data.

2. MODEL DESCRIPTION

The derivation is traditional (Hunt 1951). At any given time, let Q be the total energy available, U the internal energy of the gas, and W the work performed by the gas. Then

$$Q = U + W + \text{Losses} . \quad (1)$$

A number of estimates exist for calculating losses due to heat loss, recoil, projectile resistance, projectile rotational energy, shocked air ahead of the projectile and energy in compression of the working fluid. In small caliber guns, heat loss can be significant. However, in the current implementation for a qualitative comparison between a number of small caliber shots, losses are assumed to be similar in each firing. Thus, the "losses" term is taken to be zero.

The total available energy at the time in which a fraction $z(t)$ of a total charge mass C has been burnt in a closed vessel is

$$Q = C z(t) \int_{T_{ref}}^{T_o} c_v(T) dT \quad (2)$$

where c_v is the specific heat at constant volume of the gases at any temperature T , T_o is the flame temperature and T_{ref} is a reference temperature. Since only changes of energy will be considered, the actual value for T_{ref} is not significant.

Since work is performed in the gun, the gas temperature T is less than the flame temperature T_o , and the internal energy is given by

$$U = Cz(t) \int_{T_{ref}}^T c_v(T) dT . \quad (3)$$

The work performed by the gas is the kinetic energy of the projectile and kinetic energy of the gas. The kinetic energy of the projectile at any time is

$$KE(\text{projectile}) = \frac{1}{2} m v_p^2(x, t) \quad (4)$$

where $v_p(x, t)$ is the projectile velocity and m is the projectile mass.

The kinetic energy of the gas, $KE(\text{gas})$, is determined in a similar manner. However, since both the velocity and mass of gas can vary along the length of the gun,

$$KE(\text{gas}) = \frac{1}{2} \int_0^{x_p(t)} \rho(x, t) A(x) v_g^2(x, t) dx \quad (5)$$

where x_p is the projectile base position at time t , $\rho(x, t)$, $v_g(x, t)$ and $A(x)$ are respectively the fluid density, fluid velocity, and cross sectional area of the gun at position x .

To integrate Equation 5, the Lagrange assumption that the gas velocity $v_g(x, t)$ is linear from the breech at position 0.0 to the projectile base at x_p , with constant spatial density $\rho(t)$, that is,

$$v_g(x, t) = \frac{x}{x_p} v_p(t) \quad \text{and} \quad \frac{\partial \rho(x, t)}{\partial x} = 0 \quad (6)$$

is utilized. Then, assuming a constant area A for the gun, Equation 5, upon substitution of Equation 6, becomes

$$KE(\text{gas}) = \int_0^{x_p(t)} \frac{1}{2} \rho(t) A \left(\frac{x}{x_p(t)} v_p(t) \right)^2 dx \quad (7)$$

$$= \frac{1}{2} \rho(t) A \frac{v_p^2(t)}{x_p^2(t)} \int_0^{x_p(t)} x^2 dx \quad (8)$$

or,

$$= \frac{1}{6} \rho(t) A x_p(t) v_p^2(t) \quad (9)$$

$$KE(gas) = \frac{1}{6} C v_p^2(t) \quad (10)$$

assuming that the total charge is accelerated and uniformly distributed. Substituting Equations 2, 3, 4, and 10 into Equation 1,

$$Cz(t) \int_{T_{ref}}^{T_o} c_v(T) dT = Cz(t) \int_{T_{ref}}^T c_v(T) dT + \frac{1}{2} mv_p^2(t) + \frac{1}{6} Cv_p^2(t) \quad (11)$$

or,

$$Cz(t) \int_T^{T_o} c_v(T) dT = \frac{1}{2} mv_p^2(t) + \frac{1}{6} Cv_p^2(t) . \quad (12)$$

Assuming an average value of c_v in the temperature range, $T(t)$ to T_o yields

$$Cz(t) \bar{c}_v (T_o - T(t)) = \frac{1}{2} mv_p^2(t) + \frac{1}{6} Cv_p^2(t) . \quad (13)$$

If $v_p(t)$ can be obtained experimentally, then Equation 13 has two unknowns, z and T . A Nobel-Able covolume equation of state,

$$\bar{P}(t) \left(V_c + x_p(t) A - \frac{m_a}{\rho_a} - \frac{C(1-z(t))}{\rho_c(t)} - b C z(t) \right) = \frac{RT(t)}{MW} C z(t) , \quad (14)$$

provides a second condition on the system. In Equation 14, $\bar{P}(t)$ represents the space-mean pressure based on the Lagrange ballistic assumptions, V_c the original free chamber volume, $x_p(t)$ the projectile travel, A the cross-sectional area of the tube, m_a the mass of air in the chamber, ρ_a the density of air, $\rho_c(t)$ the working fluid or charge density which has been calculated from a compressible equation of state, b the covolume correction, R the universal gas constant, and MW the molecular weight of reaction products. The effect of air in the chamber, m_a/ρ_a , is included since ETC firings can have large initial ullage.

The equation of state for the unvaporized fluid is in the form (Gough 1989)

$$\rho_c(t) = \begin{cases} \rho_o \left(1 + \frac{(P(t) - P_o)}{K_1} \right) & \text{if } K_2 = 0 \\ \rho_o \left(1 + \frac{K_2}{K_1} (P(t) - P_o) \right)^{1/K_2} & \text{if } K_2 \neq 0 \end{cases} \quad (15)$$

where $P(t)$ is the breech pressure and ρ_o is the fluid density at the initial breech pressure P_o (ambient in these calculations) assuming that the bulk modulus, K_p , is at most a linear function of pressure,

$$K_p = K_1 + K_2 (P(t) - P_o) . \quad (16)$$

Using the standard definition of impetus, $I = \frac{RT_o}{MW}$, Equation 14 is solved for T .

$$T(t) = \frac{T_o \bar{P}(t) \left[V_c + x_p(t) A - \frac{m_a}{\rho_a} - \frac{C(1-z(t))}{\rho_c(t)} - b C z(t) \right]}{I C z(t)} . \quad (17)$$

The average value of c_v is expressed as

$$\overline{c_v} = \frac{I}{T_o(\gamma - 1)} \quad (18)$$

where γ is the ratio of specific heats.

Substituting Equations 17 and 18 into Equation 13 and solving for $z(t)$ at any time yields

$$z(t) = \frac{\frac{1}{2} m v_p^2(t) \left(1 + \frac{1}{3} \frac{C}{m} \right) + \frac{\overline{P(t)}}{(\gamma - 1)} \left(V_c + x_p(t)A - \frac{m_a}{\rho_a} - \frac{C}{\rho_c(t)} \right)}{\frac{1}{(\gamma - 1)} \left(C I + \overline{P(t)} \left(b C - \frac{C}{\rho_c(t)} \right) \right)}. \quad (19)$$

Experimental data are utilized to solve Equation 19 directly for z by providing chamber pressure from which the space-mean pressure $\overline{P(t)}$ is calculated assuming a Lagrange gradient. Experimental projectile position, $x_p(t)$, is utilized not only to calculate the projectile velocity $v_p(t)$, but also to determine the gun volume at any time. The initial charge mass, C , the bore area, A , and the projectile mass, m , are determined from the experiment. Propellant density, $\rho_c(t)$, is calculated from Equation 15. It is noted that in the calculation, each timestep is independent of any other timestep. The specification of the thermochemical values (impetus I , ratio of specific heats γ , and covolume b) is discussed in detail below.

3. NUMERICAL APPROACH

As mentioned earlier, each time step is independent of any other time step. Thus, Equation 19 can be solved algebraically for $z(t)$. However, since impetus, I , ratio of specific heat, γ , and covolume, b , are functions of $z(t)$ (see Section 5), it is necessary to iterate several times. Basically, to compute $z_{n+1}(t)$ at time t_{n+1} , values for I , γ , and b at time t_n are used in Equation 19 to determine $z'_{n+1}(t)$. New values of I , γ and b are then determined based upon $z'_{n+1}(t)$ and used in Equation 19 to determine the next approximation, $z''_{n+1}(t)$ to $z_{n+1}(t)$. This process continues until successive approximations are within the derived tolerance.

4. VALIDATION

In order to validate the inverse analysis, a 120-mm gun firing was simulated with a standard lumped parameter interior ballistic code, IBHVG2 (Anderson 1987) developed by the U.S. Army Ballistic Research Laboratory (BRL). The resulting IBHVG2 breech pressure history and projectile position were used as input to the inverse code. A comparison of the IBHVG2 calculation and the inverse analysis (ETINV) for mass consumed is shown in Figure 2. As can be seen, the inverse analysis accurately reproduces the time history of propellant mass burnt. However, as discussed elsewhere (Gough 1990), inaccuracies in the experimental data can lead to variability in the amount of mass burnt as determined by an inverse analysis. Thus, as discussed above, the inverse analysis is best viewed as a qualitative picture of the combustion process.

The ETC experimental database examined in this report consists of six 20-mm shots using titanium hydride and water, and three 30-mm shots using titanium hydride and water. All firings were performed at GT-Devices (Greig 1989), a subsidiary of General Dynamics Land Systems. A summary of the major physical parameters for the shots analyzed is shown in Table 1.

Table 1. Summary of 20-mm and 30-mm Initial Conditions

Tube Diameter	Chamber Volume	Working Fluid	Projectile Mass	Working Fluid Mass	Projectile Travel	Maximum EE Input
20 mm	72.4 cm ³	50 % TiH ₂ & 50% H ₂ O	20 g	64.0 to 64.64 g	199 cm	~500 kJ
30 mm	206.0 cm ³	50% TiH ₂ & 50% H ₂ O	100 g	168.84 g	300 cm	~400 kJ

A number of experimental measurements is available for each shot. The experimental data is used to determine plasma energy delivered to the combustion chamber, chamber pressure, and projectile position as functions of time.

As an example, the electrical or plasma energy computed from the product of the experimental voltage and current for a 20-mm shot, Shot 249, is shown in Figure 3. Pressure histories for Shot 249 are shown in Figure 4. Gages are located in the combustion chamber, and in the barrel at 13 cm, 14 cm, 18 cm, 88 cm, and 168 cm of projectile travel. The initial position of the projectile is at tube origin.

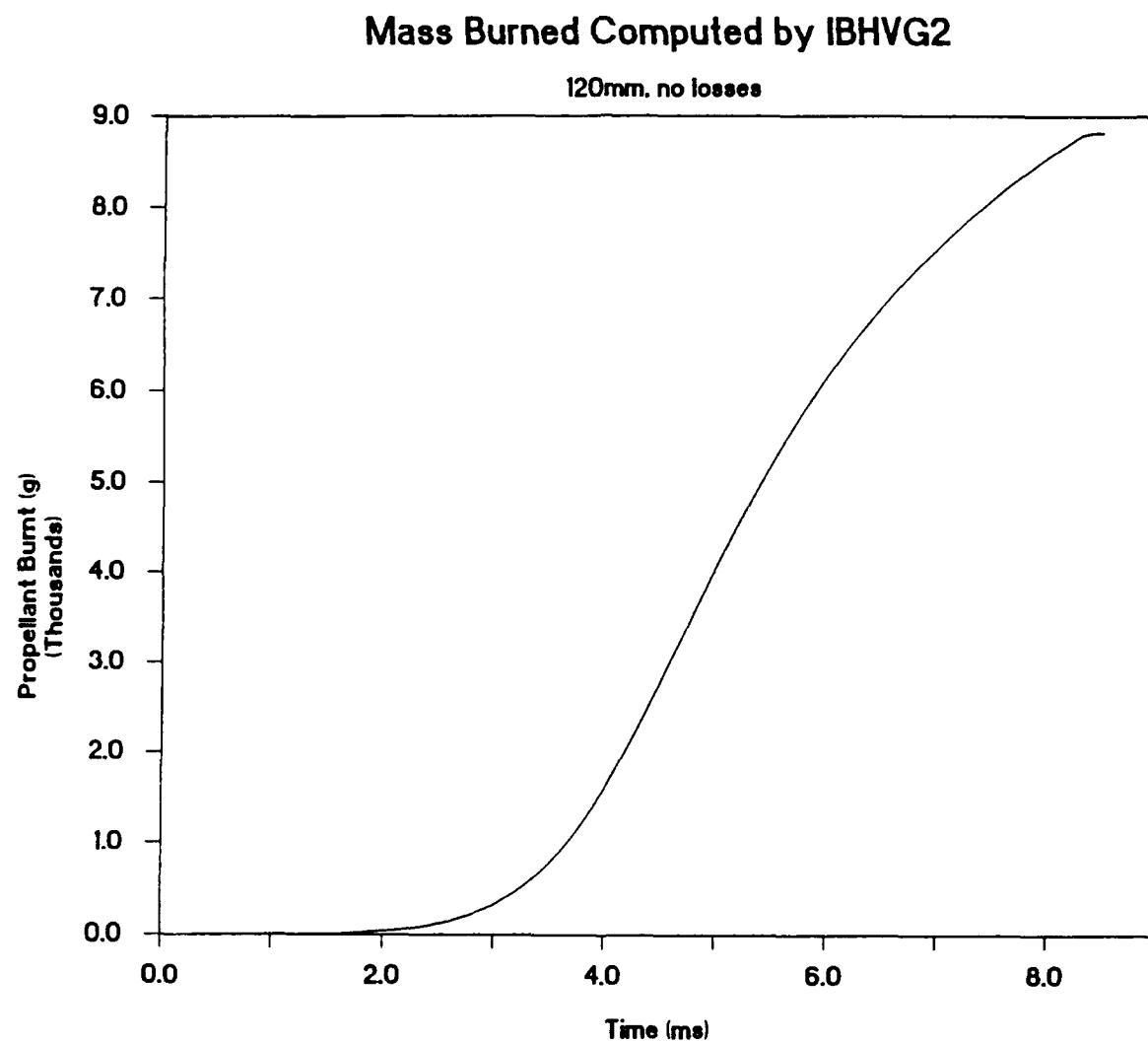


Figure 2a. Comparison of IBHVG2 Results With the Inverse Analysis.

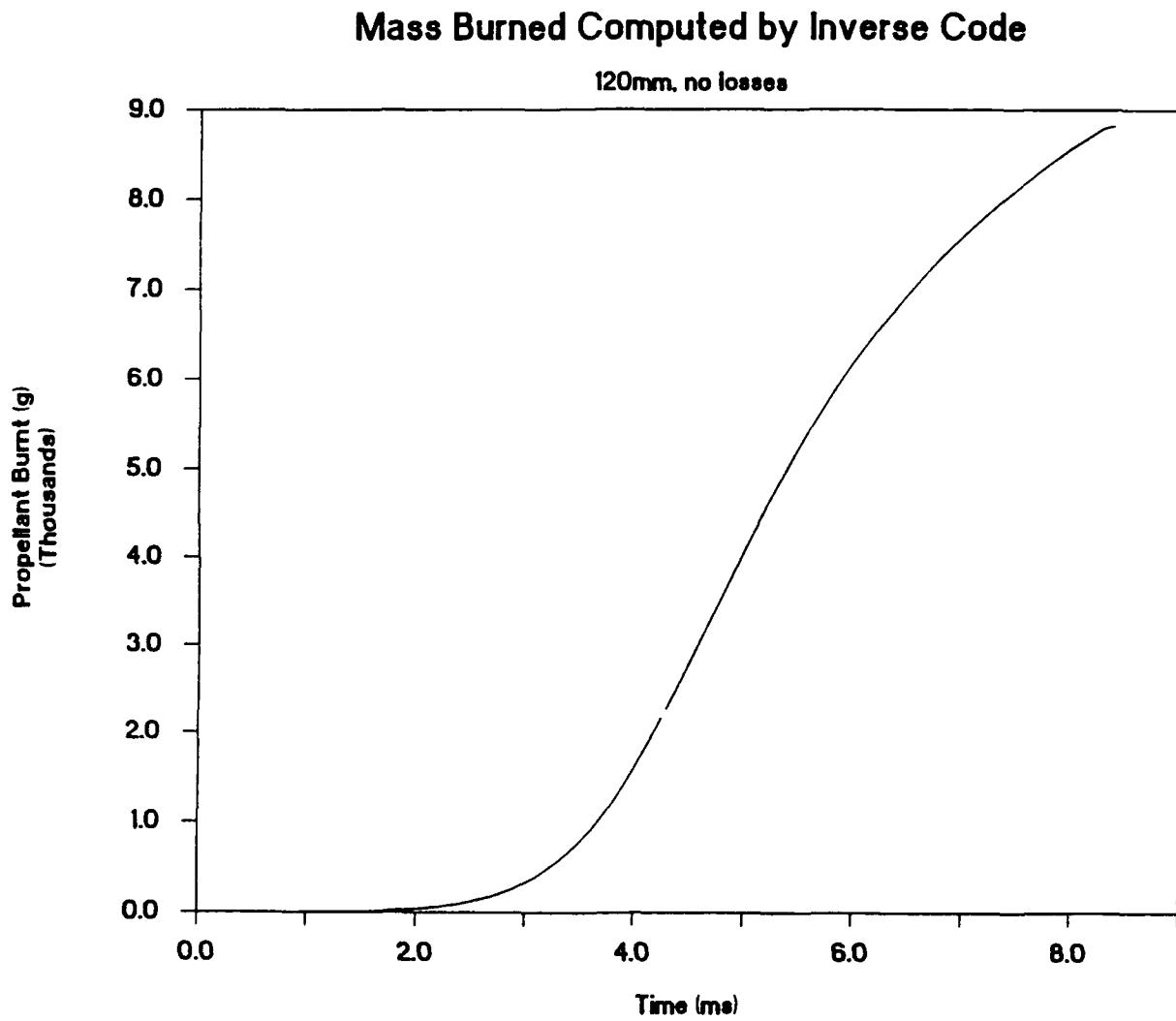


Figure 2b. Comparison of IBHVG2 Results With the Inverse Analysis.

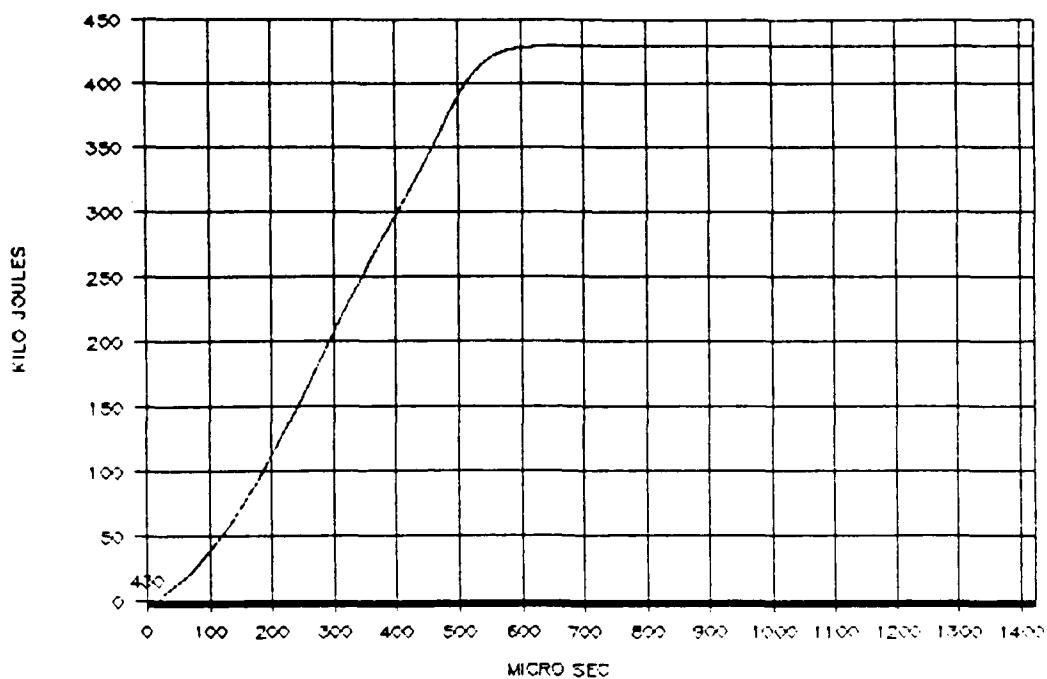


Figure 3. Electrical/Plasma Energy for 20-mm Shot 249.

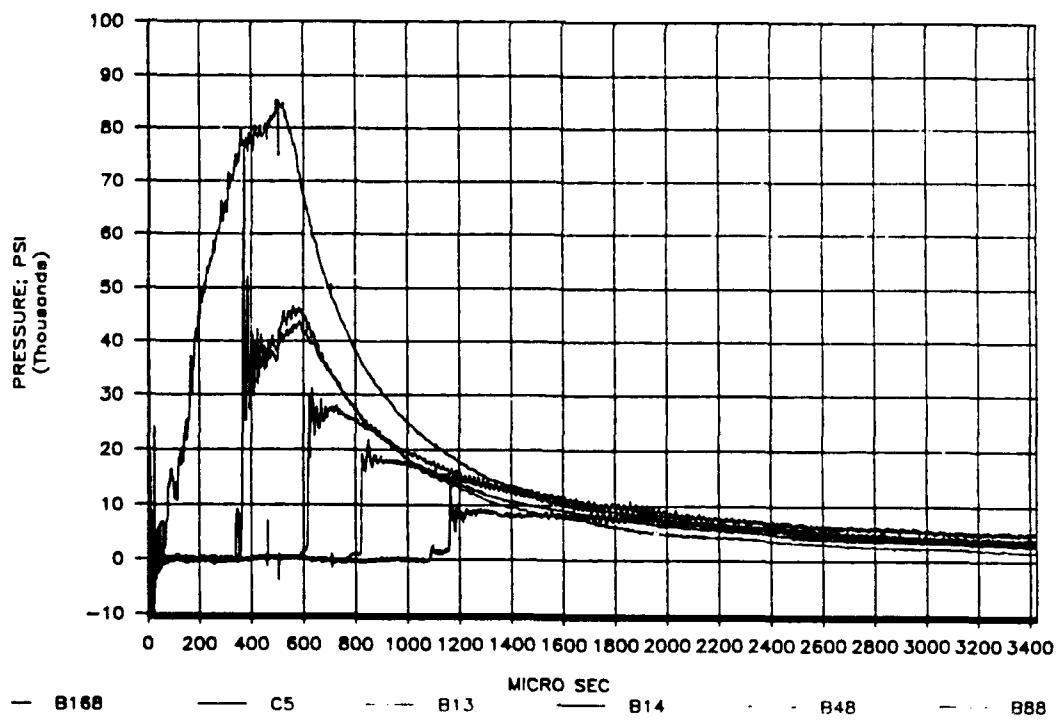


Figure 4. Recorded Pressure Histories for 20-mm Shot 249.

For the majority of firings analyzed, the chamber pressure data is smoothed since the pressure history is "noisy." To illustrate, consider the chamber pressure for Shot 249, Figure 4, which is particularly "noisy" for the first 47 μ s. To perform the smoothing, a low-pass filter is applied to the data, and the pressure history resulting from an inverse Fast Fourier Transform (FFT) is used in the analysis, a technique commonly utilized in the liquid propellant gun community. A comparison between the original data set and the data set resulting from the inverse FFT is shown in Figure 5. The filtering process is seen to maintain the characteristics of the data while removing the high frequency noise.

Projectile position is derived from arrival times at the barrel gage locations. Using the time of arrival at the barrel gage location, together with the actual gage locations, an interpolating fourth-degree polynomial of position as a function of time can be obtained. Experimental muzzle velocity, as measured by laser-velocity trap data, correlates very well with velocity predicted by the least-square fit (Greig 1989). In addition, any available radar data are utilized to confirm projectile position. However, in general, the radar data are not of sufficient fidelity to utilize in the inverse model. The polynomial method of determining projectile travel distorts the initial estimate of projectile motion prior to the first pressure probe since it is an extrapolation, as shown in Figure 6 for Shot 249. The projectile begins motion at 73 μ s, and the projectile travel is negative from 73 μ s to 133 μ s. To eliminate negative projectile travel in the analysis, a quadratic fit is applied over the time from 73 μ s to 133 μ s using zero travel at 73 μ s and the calculated travel at 133 μ s. The resulting estimated projectile travel history is shown in Figure 7 for Shot 249. However, this procedure calls into question results obtained for approximately the first 15% of the analysis as a function of time.

The accuracy of the inverse analysis is dependent on accurate experimental data for plasma energy delivered to the combustion chamber, chamber pressure history, and projectile travel. Thus, since much of the needed information from the titanium hydride and water firings is inferred, as opposed to directly measured, the analysis of these firings is useful only as a comparison between experiments with similar initial conditions (i.e., gun geometry, plasma energy, etc.). An accurate estimation of gas generation rate will require precise experimental data.

5. THERMOCHEMISTRY

The specification of the thermochemical properties of the working fluid must consider the input of the plasma. Therefore, a series of BLAKE (Freedman, private communication) runs are performed with

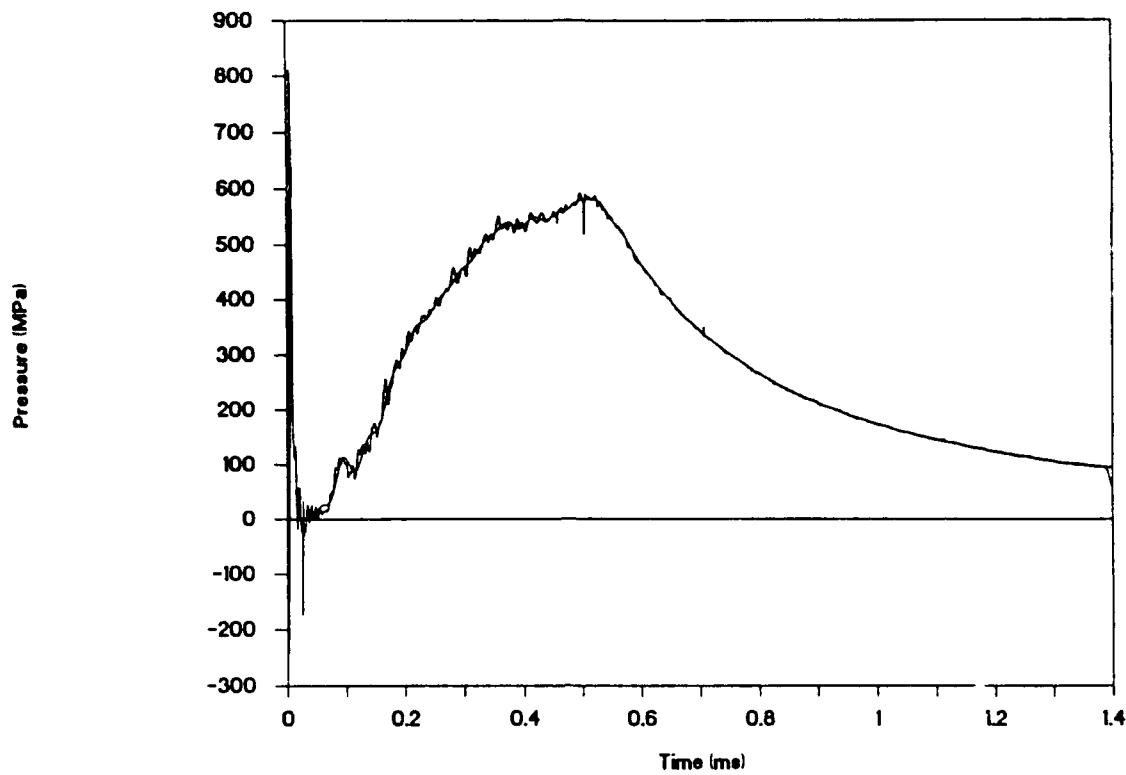


Figure 5. Comparison Between Chamber Pressure Gage History and Filtered Chamber Pressure Gage History for 20-mm Shot 249.

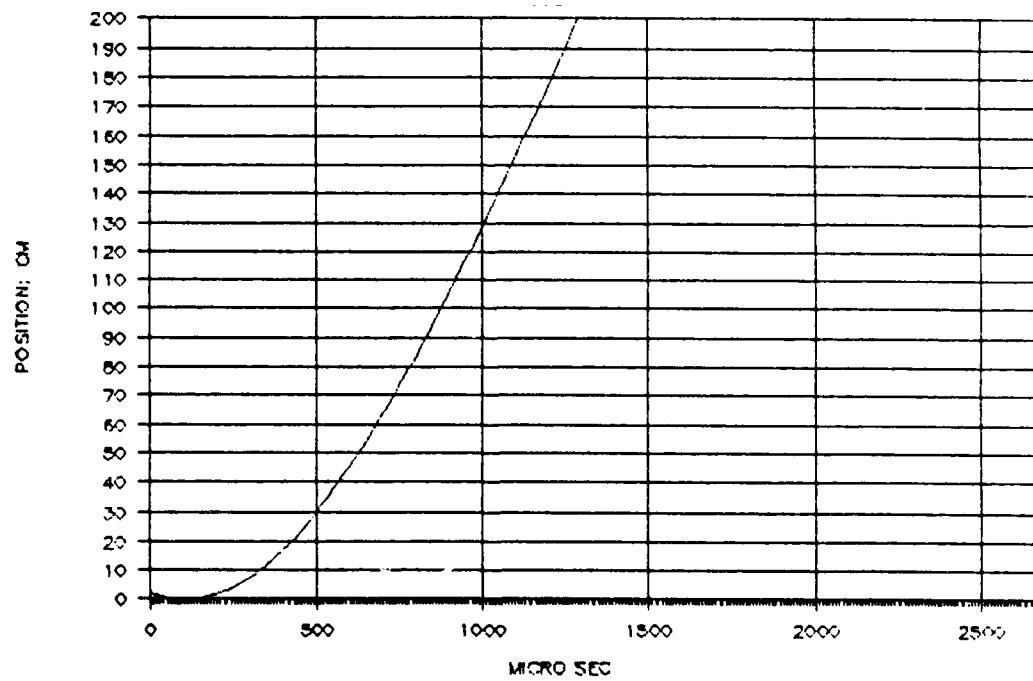


Figure 6. Projectile Position Derived From a Polynomial Least-Squares Fit to Barrel Gage Arrival Times for 20-mm Shot 249.

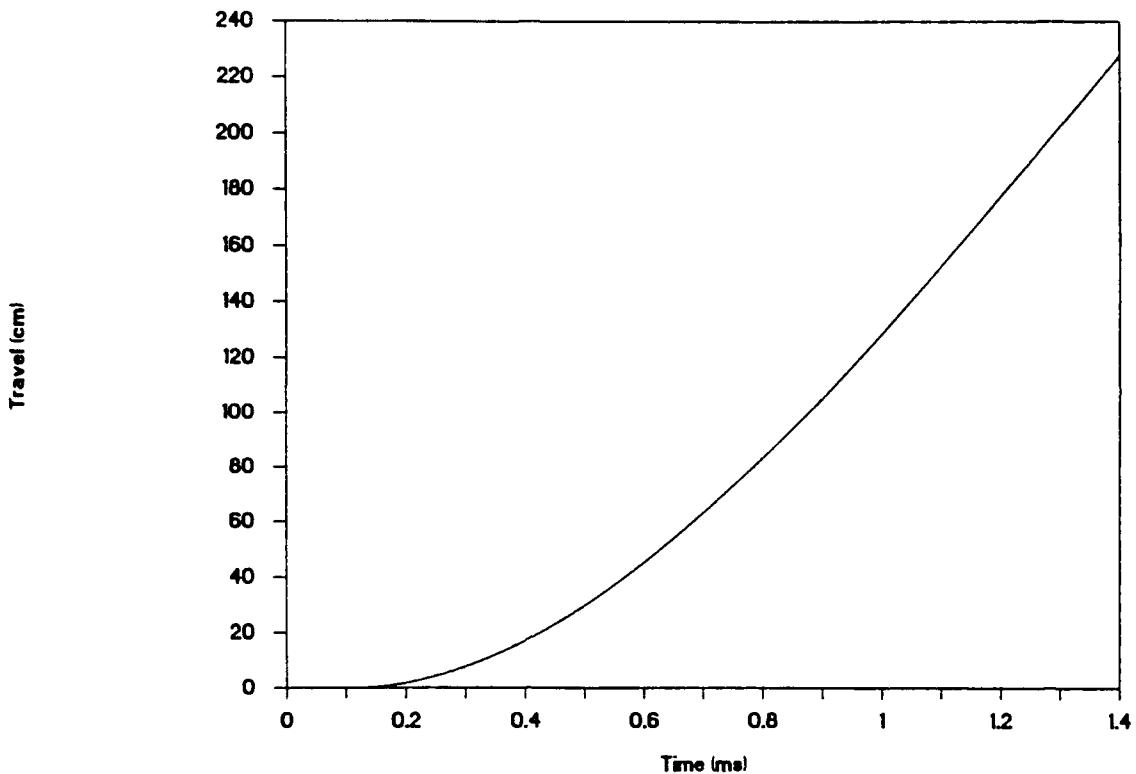


Figure 7. Projectile Position Derived From a Polynomial Least-Squares Fit to Barrel Gage Arrival Times for 20-mm Shot 249 After 133 μ s, Together With a Quadratic Fit From 73 μ s to 133 μ s.

varying amounts of plasma energy input (Bunte and Oberle 1989). In the BLAKE calculations, the plasma energy is assumed to mix uniformly with some amount of working fluid, and the ratio of electrical energy input to working fluid mass is referred to as the electrical energy density. Based on the electrical energy density, BLAKE then defines an impetus, ratio of specific heats, temperature and molecular weight for the mixture. In the inverse analysis, the plasma energy is assumed to mix only with the dissociated working fluid as determined iteratively from Equation 19. Since the BLAKE entries are not defined above approximately 6,000 K where ionization would occur, the impetus values are extended with a linear regression line to define electrical energy densities outside the table range.

Impetus for a mixture of 50% TiH_2 and 50% H_2O as a function of electrical energy density is shown in Figure 8 for the BLAKE calculations and is denoted by the square boxes. The linear regression line is shown in Figure 8 as well, and is given by

$$Impetus = 134.238 * (EE\ density) + 424.69.$$

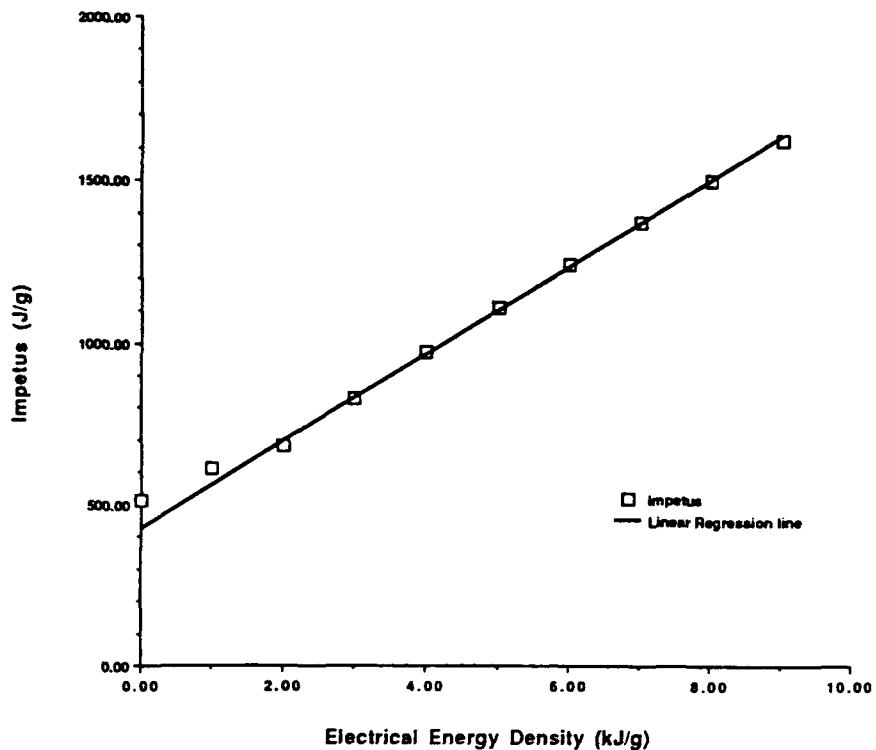


Figure 8. Impetus of $\text{TiH}_2/\text{H}_2\text{O}$ With Electrical Energy Added.

The variable thermochemistry values are shown in Table 2. As can be seen from an examination of Table 2, the values of gamma and the covolume for electrical energy densities producing gas temperatures above 5,000 K are held constant at the last BLAKE calculation at 9 kJ/g. Although not accurate, better thermochemical data does not exist at the present time.

6. RESULTS OF INVERSE ANALYSIS

The inverse analysis assesses ballistic control exhibited in the experiment by inferring the relationship between electrical energy added to the system by the plasma and the amount of working fluid consumed. The delivery of electrical energy to the system is first discussed for the experimental shots. Results of the inverse analysis are then shown for 20-mm and 30-mm gun data with working fluid titanium hydride and water.

Electrical energy input in kilojoules vs. time in milliseconds is shown in Figure 9 for the six 20-mm firings (Shots 240, 249, 250, 257, 258, and 259). The shape of the curves is quite similar with a variation in pulse length and total energy. The 30-mm experiments are firings in which initial conditions and the

Table 2. Thermochemistry of 50% TiH₂ and 50% H₂O

EE Density (kJ/g)	Temperature (K)	Impetus (J/g)	Gamma (-)	Covolume (cm ³ /g)
0	1,627	511	1.1685	0.655
1	1,950	612	1.1685	0.655
2	2,162	679	1.2722	0.655
3	2,630	826	1.2553	0.668
4	3,078	969	1.2443	0.675
5	3,502	1,106	1.2370	0.681
6	3,899	1,239	1.2325	0.690
7	4,265	1,368	1.2302	0.702
8	4,604	1,495	1.2294	0.717
9	4,917	1,622	1.2299	0.735
10	—	1,767	1.2299	0.735
20	—	3,109	1.2299	0.735
30	—	4,451	1.2299	0.735
40	—	5,794	1.2299	0.735
50	—	7,136	1.2299	0.735
60	—	8,478	1.2299	0.735
70	—	9,821	1.2299	0.735
80	—	11,163	1.2299	0.735
90	—	12,506	1.2299	0.735
100	—	13,848	1.2299	0.735

delivery of electrical energy are nearly the same. Thus, these shots (Shots 39, 40, and 43A) form a repeatability series for this gun configuration. As shown in Figure 10, approximately 350 kJ of electrical energy is delivered as a simple ramped input over approximately 1.4 ms.

To assess the dependence of working fluid consumed on plasma energy input, the results are presented as groups of normalized electrical energy input vs. normalized working fluid consumed. The normalized curve (Figures 11 and 12) is obtained by dividing electrical energy by the maximum electrical energy

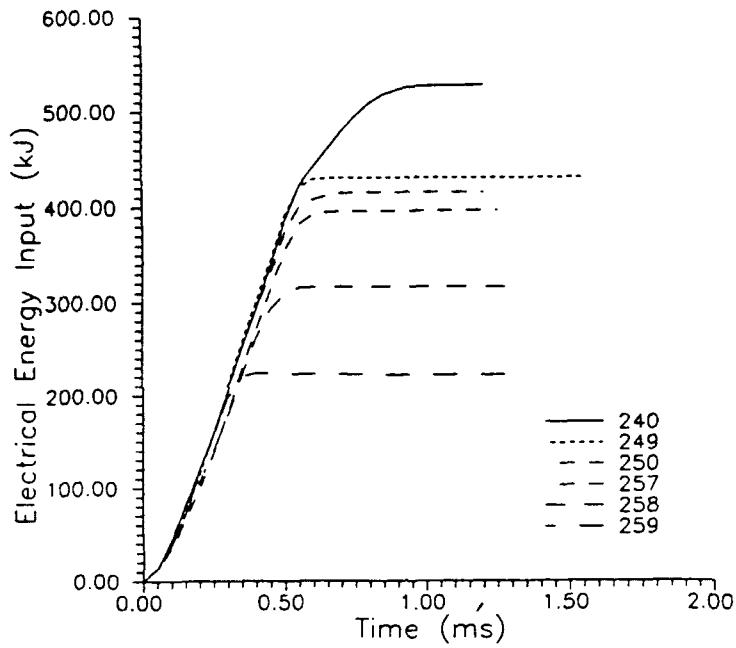


Figure 9. Electrical Energy Input (kJ) as a Function of Time (ms) for 20-mm Gun Firings.

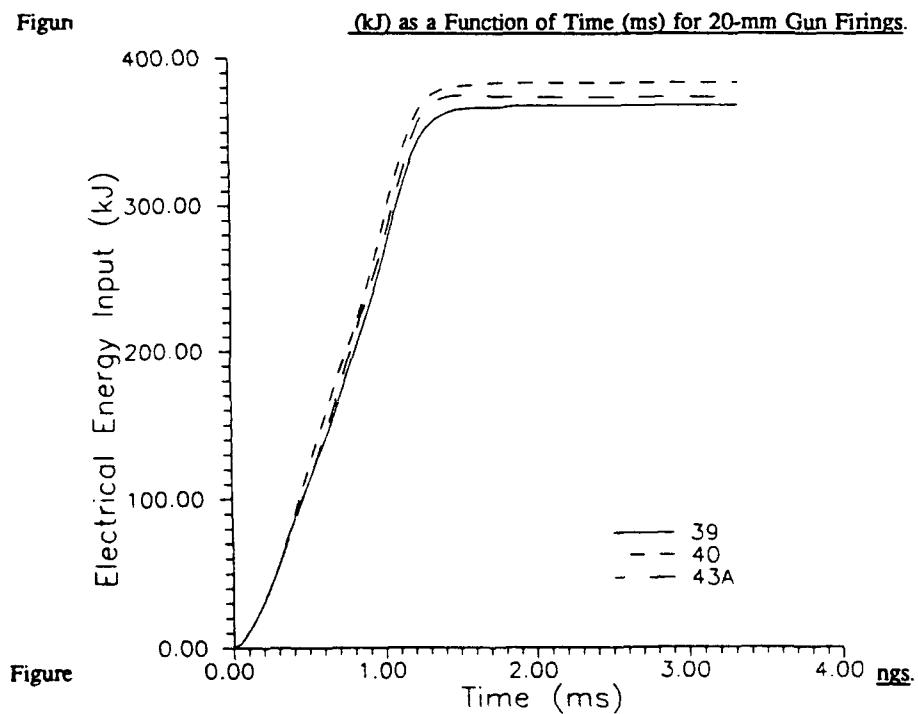


Figure 10. Electrical Energy Input (kJ) as a Function of Time (ms) for 30-mm Gun Firings.

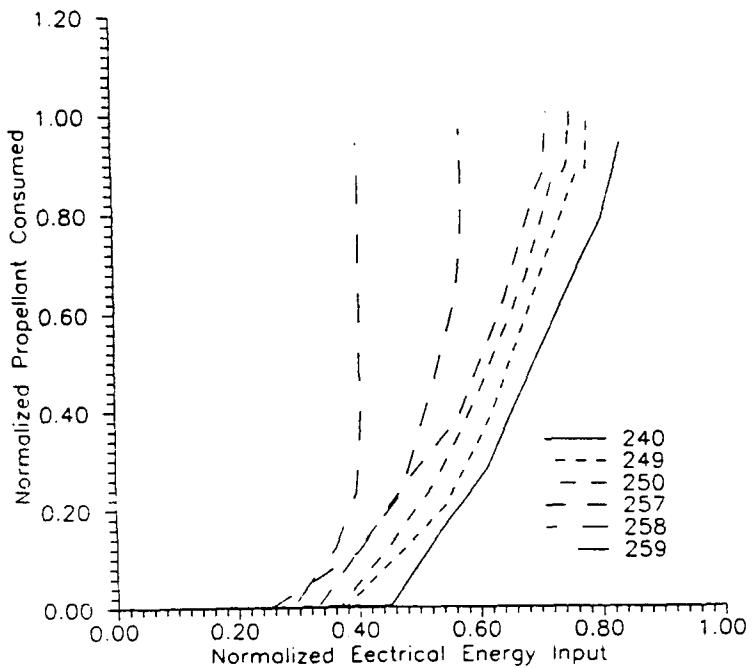


Figure 11. Normalized Electrical Energy Input vs. Normalized Working Fluid Consumed for 20-mm Gun Firings.

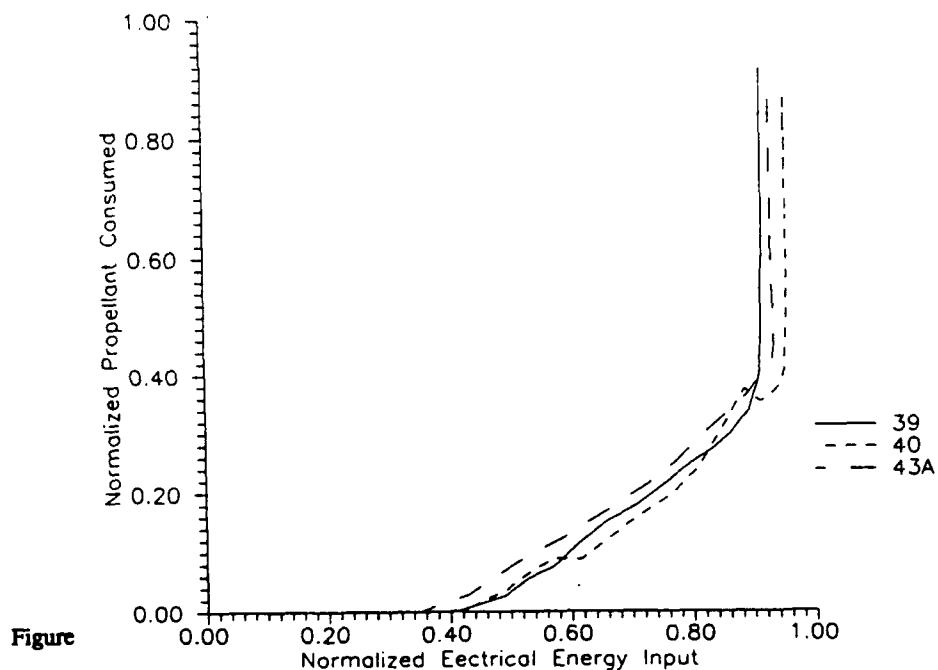


Figure 12. Normalized Electrical Energy Input vs. Normalized Working Fluid Consumed for 30-mm Gun Firings.

input and the mass consumed by the maximum mass of working fluid in the experiment. The computed mass of working fluid consumed is shown in Appendix B for each shot, with the sample input/output in Appendix A.

The results for the 20-mm shots with titanium hydride and water as the working fluid are shown in Figure 11. From Figure 9 the electrical energy input is a simple ramp. Although the mass of working fluid consumed (Figure 11) does indicate some linearity as a function of electrical energy, the results provide no evidence that the plasma energy input drives the ballistic response for the entire ballistic cycle.

The 30-mm shots using titanium hydride and water as the working fluid are shown in Figure 12. These shots form a set of repeatability experiments. As shown in Figure 10, the approximately 350 kJ of electrical energy is deposited uniformly over approximately 1.2 ms in each experiment. As can be seen in Figure 12, the working fluid response is similar in all three experiments. As in the 20-mm experiments, although the plasma energy is applied uniformly, the rate of working fluid mass consumed appears to increase during the ballistic cycle. Although the mass fraction of working fluid consumed appears to occur similarly in the experiments, it is not evident that the plasma controls the ballistic process.

In both experimental data sets, an increase in the rate of working fluid consumed over time is observed. In order to identify the role of plasma energy as the driving mechanism in the gas generation rate, shots in which the initial plasma input is substantially varied should be fired and compared.

An analysis of several firings with water as the working fluid was attempted. It is possible to devise an extended thermochemical description of the mixture of water and electrical energy similar to Table 2. However, as demonstrated by Gough (1990) and verified in the analysis of experimental data, the dependence of pressure on the fraction of working fluid consumed is weak for endothermic fluids for all electrical energy densities. As opposed to exothermic fluids, the possibility of multiple roots and bifurcation in the inverse analysis makes water firings unsuitable for inverse analysis. Thus, these firings are not further discussed in this report.

7. SURFACE AREA RATIO

A second method to investigate control of the ballistic process is to ascertain the surface area of the reacting working fluid. If the process is not controlled, it would be expected that the total reacting surface

area would display large fluctuations. To determine an apparent surface area, the experimental breech pressure and working fluid mass consumed (as computed from the inverse analysis) are used to compute a surface area ratio (current surface area to initial surface area) under the assumption of a pressure dependent combustion law for the working fluid reaction. Although the results are qualitative, the ratio provides some insight into the behavior of the surface which is in contact with the hot gases. Surface area ratios in solid propellants are well behaved.

A pressure dependent burn rate of JA2 propellant ($r = 0.12 P^{0.95}$, r in cm/s) and an initial surface area equal to the cross-sectional area of the chamber are assumed. Then for each percent mass consumed, the ratio of the current to the initial surface area can be computed. The selection of the initial surface area as the cross-sectional area of the chamber is arbitrary. However, changing the value of the initial surface area preserves the shape of the surface area ratio curve but changes its magnitude. Thus, the surface area ratio curves should not be viewed in terms of absolute magnitude but only in terms of characteristic shape. The results are similarly affected by the choice of burn rate law. Figure 13 shows the surface area ratio for three 20-mm firings, Shots 240, 249, and 259, with titanium hydride and water as the working fluid. For the first 50% of the mass consumed the ratios show minor fluctuations except for the early portions of the graph where the data is questionable due to the inaccuracies in the early portion of projectile travel. Unfortunately, the surface area ratios fluctuate sharply after approximately 50% of the working fluid mass has been consumed, especially Shot 249. In the experiments, the plasma continues to enter the chamber until almost all of the working fluid has been consumed as seen in Figure 11. Thus, the working fluid surface area appears to be well behaved only initially.

For comparison, the geometry of an inhibited, monolithic grain with dimensions suggested by the initial working fluid configuration is theoretically burned under the same pressure-dependent conditions. The surface area ratio as a function of percent mass consumed is shown in Figure 13 and is seen to be progressive and well-behaved.

8. CONCLUSIONS

An inverse analysis has been presented as one method of assessing ballistic control exhibited in ETC experimental gun firings. The analysis attempts to determine the decomposition or gas generation rate necessary to satisfy an energy balance equation as gleaned from available experimental data. The quantitative values of working fluid mass consumed are dependent on accurate experimental breech

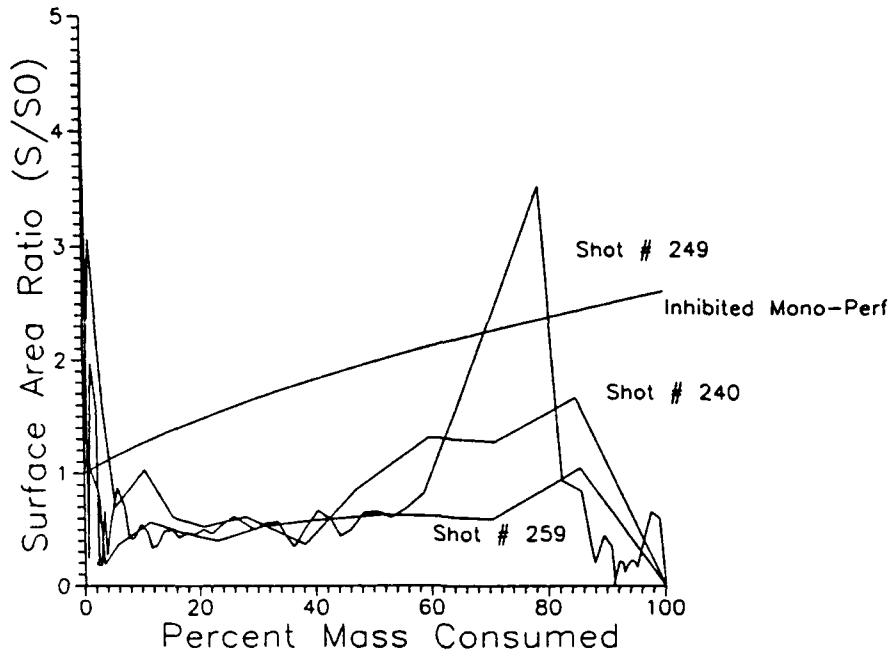


Figure 13. Surface Area Ratio for 20-mm Shots 240, 249 and 259 Compared to Inhibited, Monolithic Grain.

pressure measurements and projectile position as well as the assumption of the form of the pressure gradient.

The analysis was applied to 20-mm and 30-mm experimental firings (rear plasma injection) using titanium hydride and water as the working fluids. The results of the analysis are viewed as qualitative for these data sets and suggest:

- (1) For the firings analyzed, there is little evidence to indicate that the electrical energy input plays a dominant role in the amount of working fluid consumed.
- (2) A large fluctuation in surface area occurs for the titanium hydride and water system when approximately 50% of the mass has been consumed regardless of the presence or absence of plasma energy in the configuration analyzed.

- (3) Accurate measurement of projectile position through in-bore radar is needed to accurately establish the volume behind the projectile.
- (4) The potential coupling between plasma energy input and working fluid mass consumed is obscured by the lack of comparable data sets in which the plasma energy input history is significantly varied.
- (5) Additional work is needed in defining the thermochemistry of working fluid/electrical energy combinations.

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9. REFERENCES

Anderson, R. D., and K. D. Fickie. "IBHVG2—A User's Guide." BRL-TR-2829, U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, MD, July 1987.

Bunte, S. W., and W. F. Oberle. "A Thermochemical Analysis of Proposed Working Fluids for Electrothermal Guns." BRL-TR-3000, U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, MD, June 1989.

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Gough, P. "Numerical Simulation of Electrothermal Gun Interior Ballistics." 27th JANNAF Combustion Meeting, Frances E. Warren Air Force Base, Cheyenne, WY, 5–9 November 1990.

Greig, J. R. "An Analysis of Fifty Shots on the 20-mm Electrothermal Gun for Reproducibility and Energy Dependence." Interim Report GTD 89-8, GT-Devices, Inc., Contract No. DAAA15-86-C-0015, 23 June 1989.

Hunt, F. Internal Ballistics. New York: Philosophical Library, Inc., 1951.

White, K. Private communication. U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, MD.

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APPENDIX: A

SAMPLE INPUT

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Enter the file containing input file names.

Inverse Electrothermal Gun Code

Pressure-time file:250tvp.IN
Proj motion-time file:250tvpp.IN
Proj travel-time file.

Electrical energy-time file:250tvce.IN
Initial data file:250init.IN
Chamber volume (cm³)= 72.40000
Tube diameter (cm)= 2.1 Area (cm²)= 3.46361
Projectile position (cm)= 0.00000
Projectile mass (kg)= 0.02
Working fluid mass (g)= 64.64000
Initial working fluid density (g/cm³)= 1.59000
Tolerance required in mass consumed= 0.00100
Time start (sec)=0.00000000
Time increment (sec)=0.00005000
Time end (sec)=0.00120000
Initial guess for mass consumed (g)= 0.10000
Initial value of beta, fraction of wf moving (-)= 1.00000
Mass of air initially in chamber (g)= 0.03750
Bulk modulus of WF at atmosphere (MPa)=5000.00000
Derivative of bulk modulus wrt pressure (-)= 8.00000

Thermochemical data file:tihextra.prn

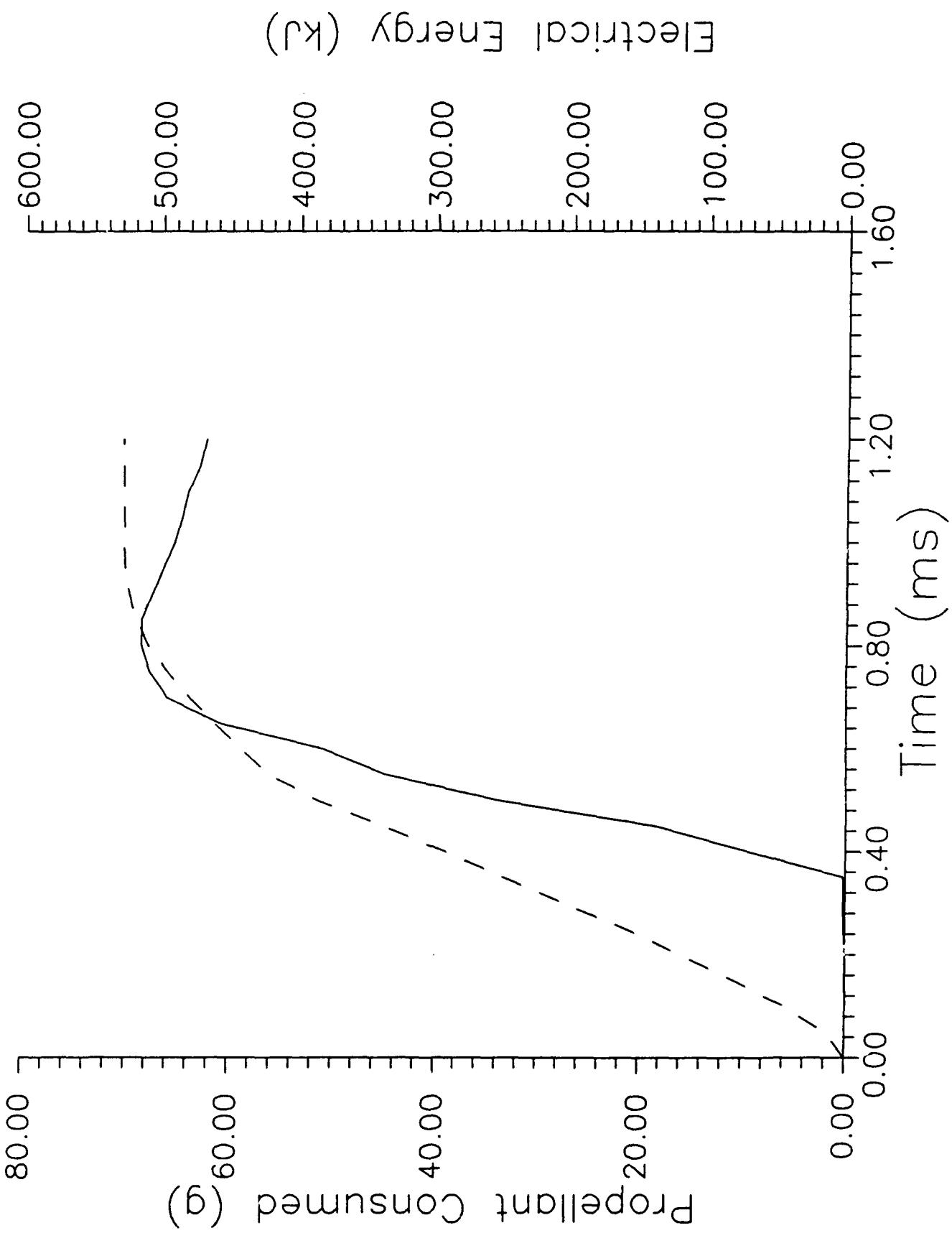
TIME (ms)	CHAM PR (MPa)	BASE PR (MPa)	PROJ TRAV (cm)	PROJ VEL (cm/s)	EL EN DEN (MJ/kg)	CUM WF (g)
0.00	0.10	0.04005	0.0000	0.00	0.000	0.00000
0.05	2.89	1.15726	0.3916	7831.56	19259.860	0.00079
0.10	98.12	39.29342	0.7832	7831.56	2101.635	0.02080
0.15	200.20	80.17240	1.1747	7831.56	1811.112	0.04470
0.20	338.07	135.38190	1.5663	27364.79	1433.635	0.08227
0.25	413.63	165.64180	3.9112	55843.03	1198.416	0.12971
0.30	493.50	197.62530	7.1506	73255.77	1039.150	0.19483
TIME-	0.00035	NO CONVERGENCE				
0.40	573.84	229.79470	16.1227	105250.30	17.629	16.52764
0.45	577.92	231.42860	21.7618	119858.60	11.768	28.05256
0.50	588.95	235.84870	28.1085	133558.50	8.616	43.34926
0.55	559.01	223.85940	35.1177	146363.10	7.105	56.13565
0.60	473.38	189.56690	42.7448	158286.10	7.172	56.85619
0.65	403.04	161.39790	50.9463	169340.30	7.109	57.92583
0.70	355.40	142.31970	59.6788	179538.80	6.588	62.86549
0.75	306.18	122.61100	68.9001	188895.20	6.544	63.38555
0.80	263.75	105.61900	78.5683	197422.40	6.623	62.64100
0.85	235.21	94.18995	88.6424	205134.10	6.418	64.93068
All fluid consumed.						
Solution continues to balance energy.						
0.90	213.39	85.45189	99.0817	212043.00	6.418	66.28542
0.95	190.69	76.36062	109.8466	218163.30	6.418	66.49628
1.00	171.73	68.76966	120.8980	223505.80	6.417	66.69440
1.05	156.52	62.67997	132.1973	228086.30	6.417	67.08662
1.10	143.31	57.38857	143.7066	231917.30	6.417	67.33691
1.15	130.72	52.34921	155.3890	235012.50	6.416	67.08495
1.20	119.08	47.68684	167.2078	237381.90	6.416	66.46645

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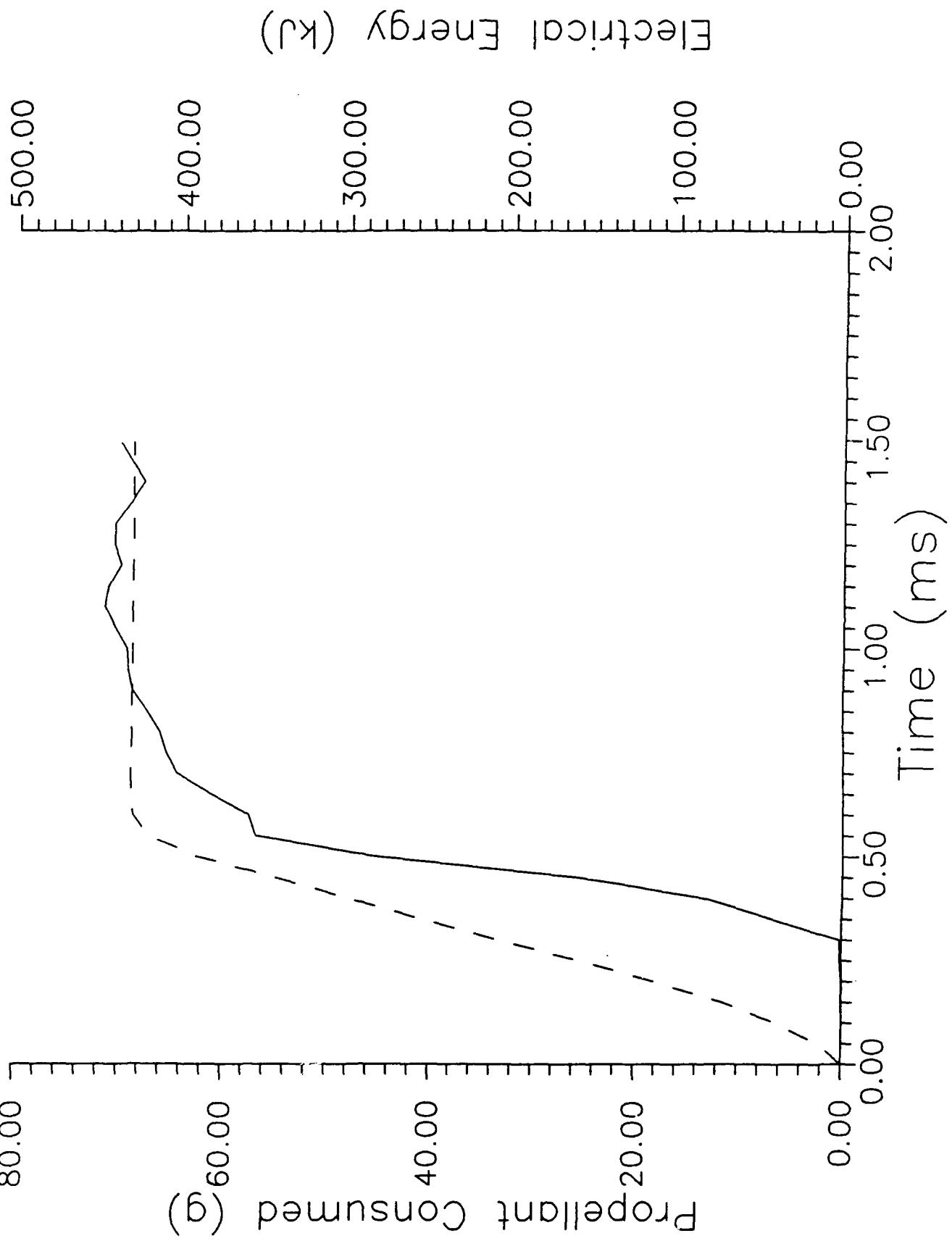
APPENDIX B:
INVERSE SIMULATION OF 20-MM AND 30-MM FIRINGS OF T:H₂/H₂O

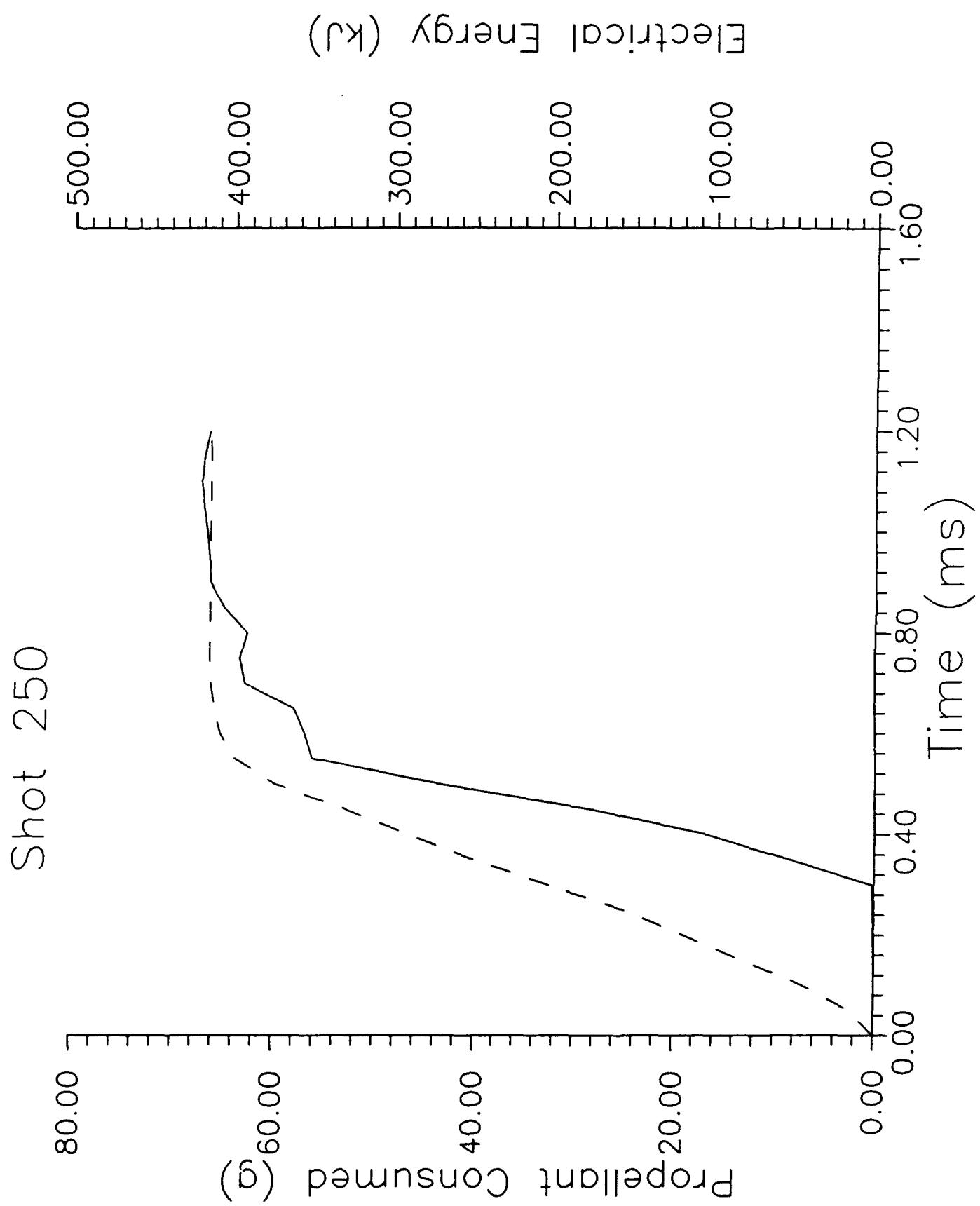
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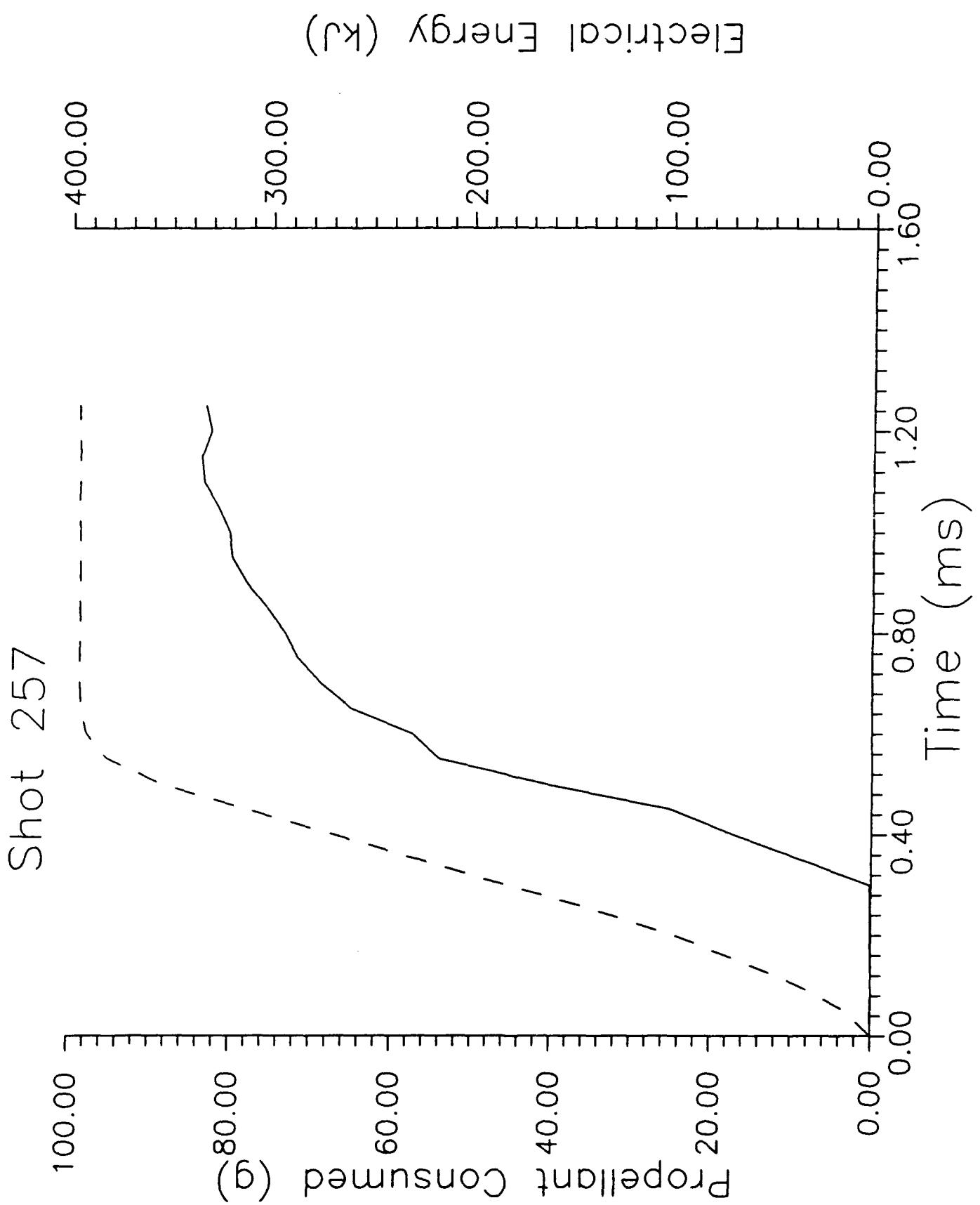
Shot 240



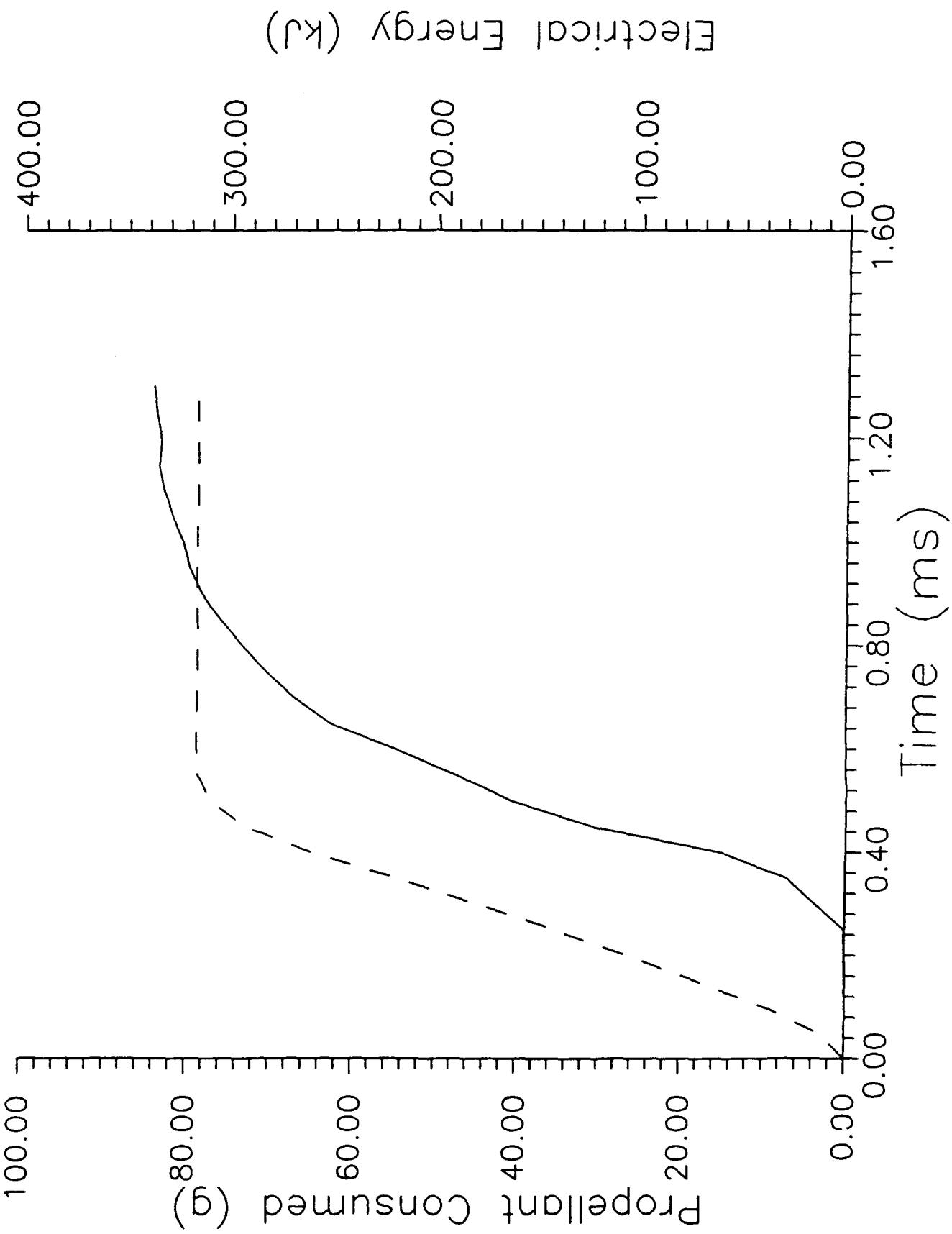
Shot 249



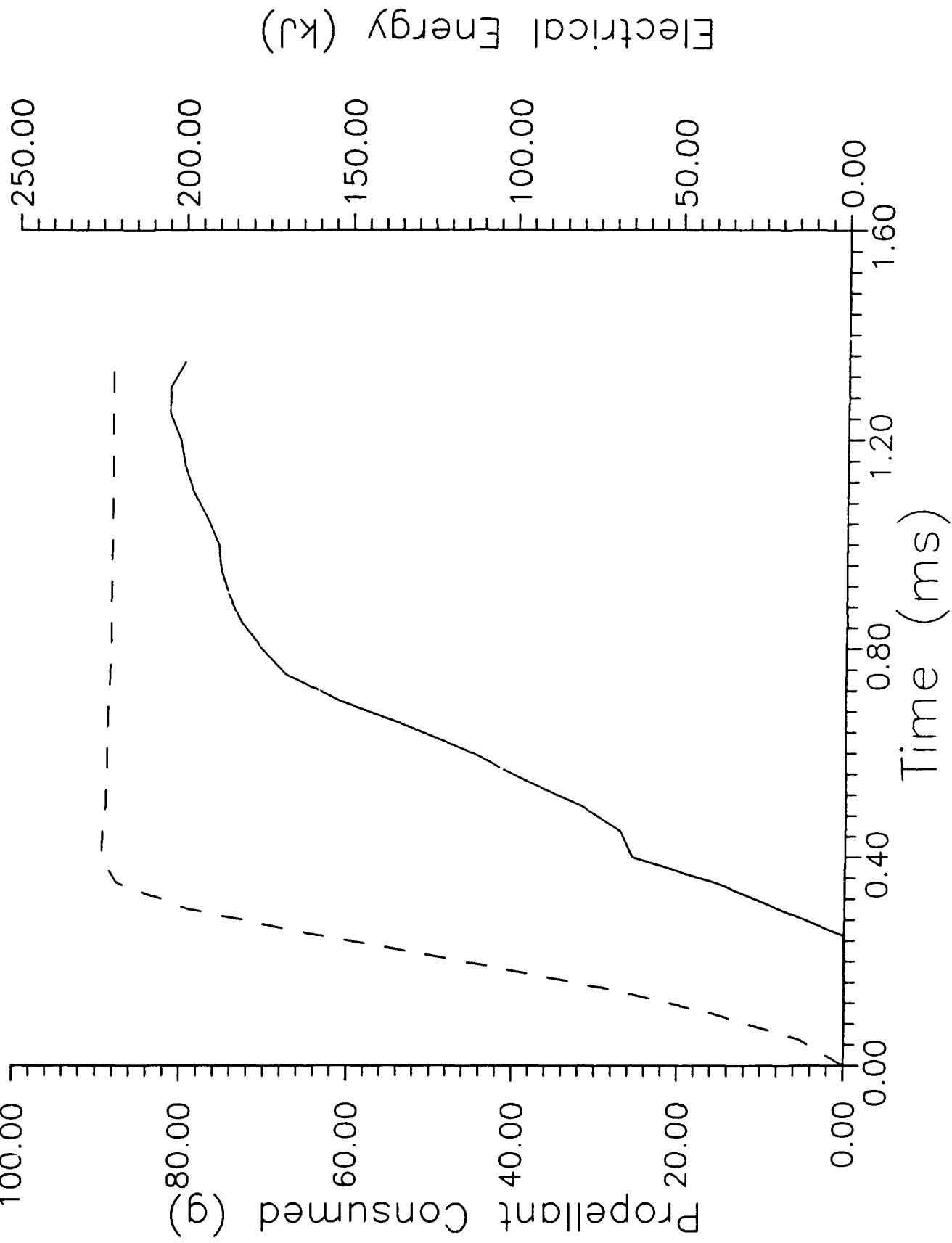


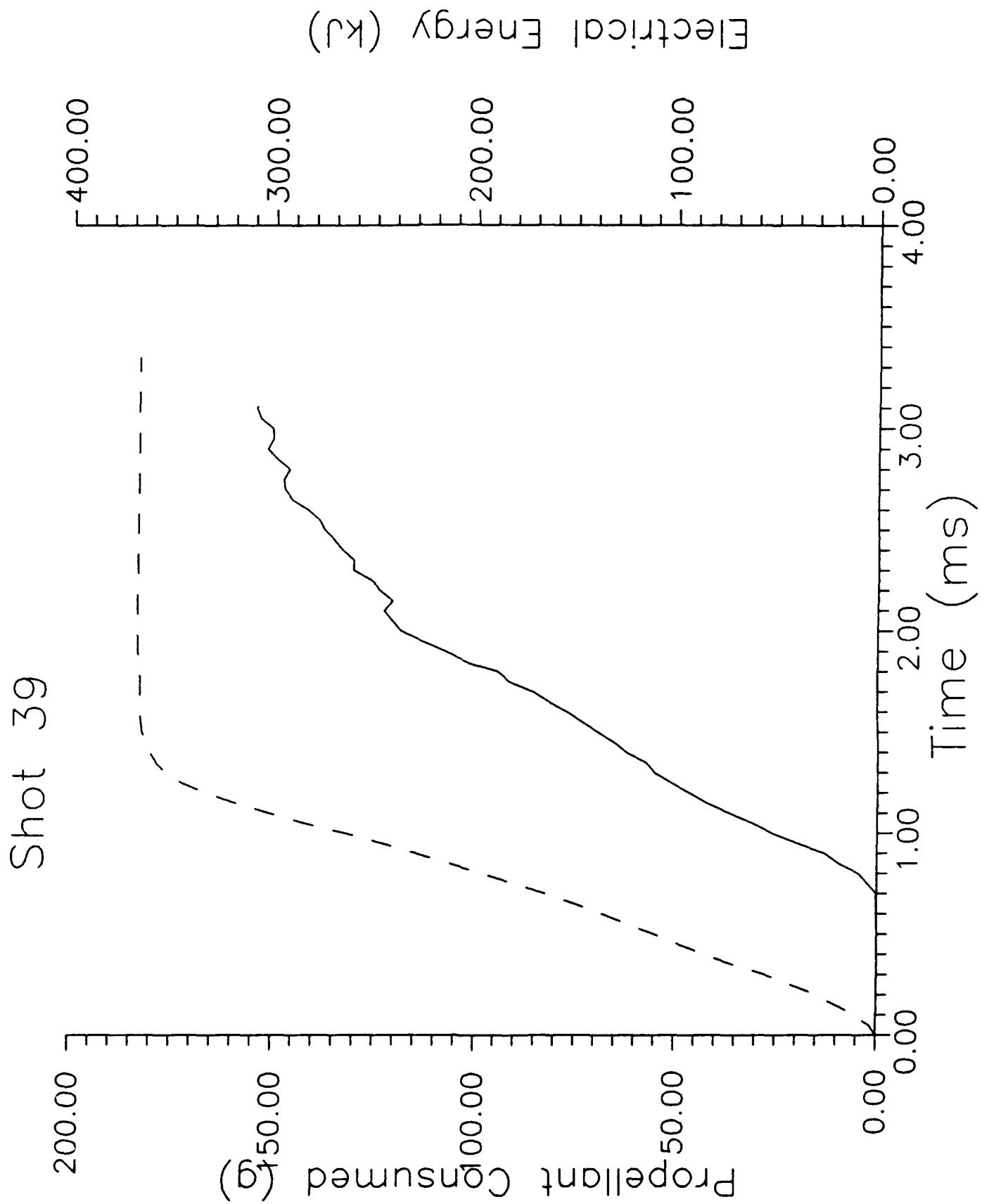


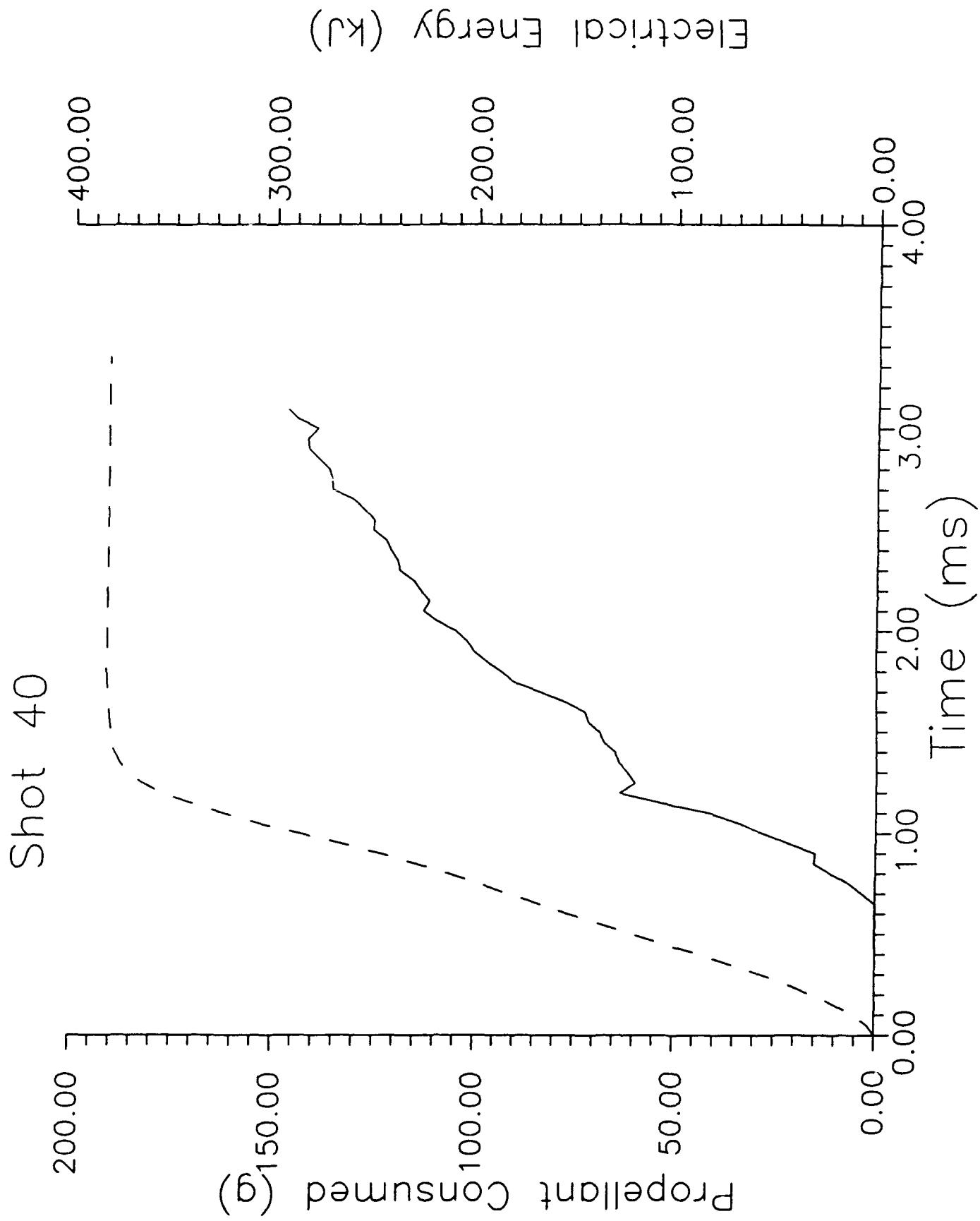
Shot 258

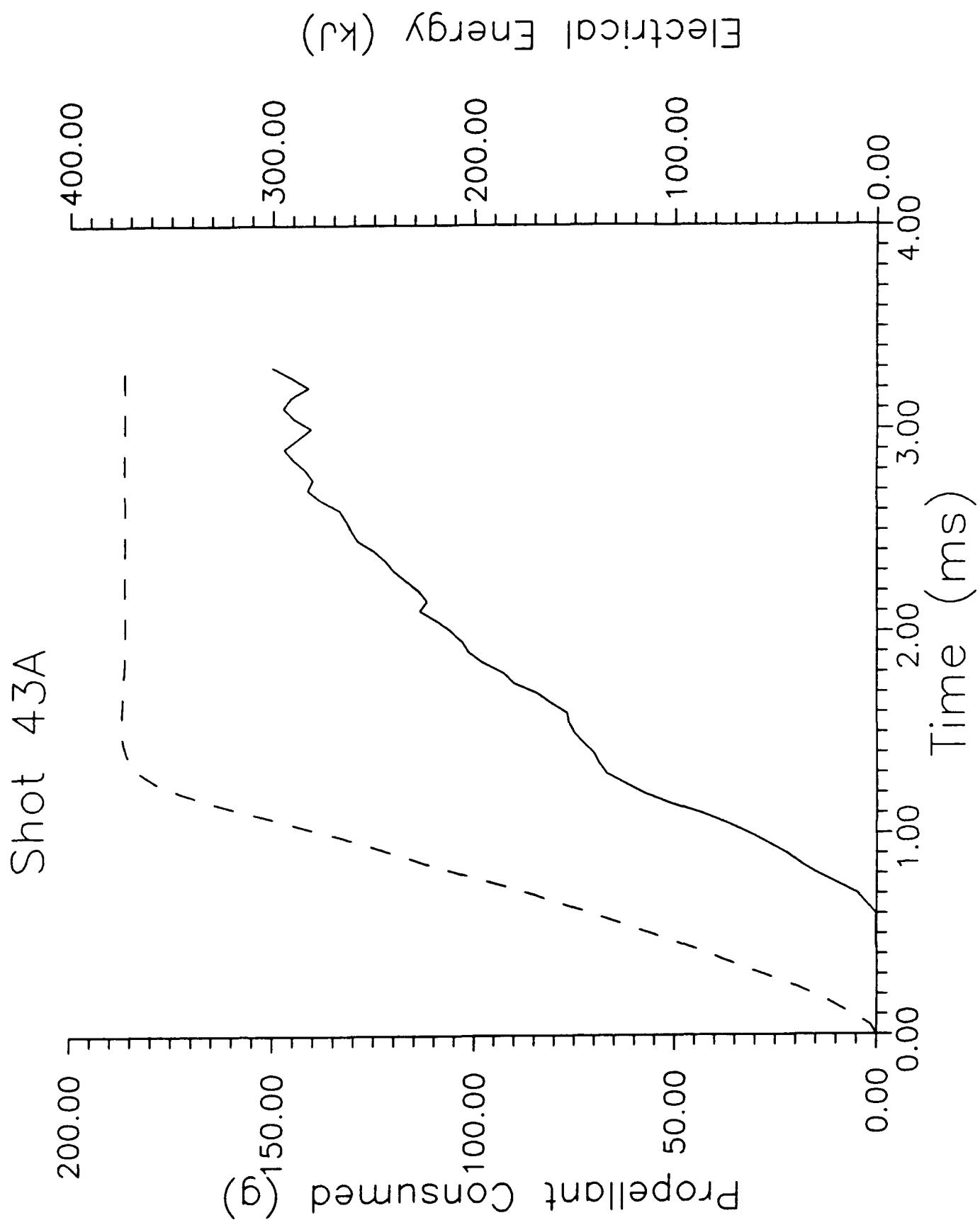


Shot 259









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APPENDIX C:
SOURCE CODE LISTING

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PROGRAM ETINVBC

```
C
C ADD COMPRESSION OF WORKING FLUID - JULY 1990
C
C CONSIDER BETA--AMT OF FLUID WHICH MOVES
C APRIL 1990
C INVERSE PROGRAM TO CALCULATE INTERACTION RATE
C OF WORKING FLUID AND PLASMA FROM ET DATA
C ASSUMING LAGRANGE PRESSURE GRADIENT
C
C TYPE ETINVBC (WAIT FOR QUESTION ABOUT INPUT FILE!!)
C

IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /NAME/ PRESIN, TRAVIN, ELECIN, THERIN, INITIN
COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1 TRTIM (1:NPT), TRAV (1:NPT),
2 VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
COMMON /OUT/ WFTIM (NPT), WFCUM (NPT)
COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
1 PROJI, PROJW, TOL, TIMINC,
2 TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1 ELECEN, TEMP, RIMPET, GAMMA,
2 COVOL, WF1, WF2, ELDEN, SPMPR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
COMMON /THERMO/ ELDEN1 (1:NPTT), TEMP1 (1:NPTT), RIMP1 (1:NPTT),
1 GAMMA1 (1:NPTT), COVOL1 (1:NPTT)

C
CHARACTER*20 ETIN, PRESIN, TRAVIN, ELECIN, THERIN, INITIN
C
WRITE (*, 6000)
6000 FORMAT(10X,' Enter the file containing input file names.')
READ (*, 5000) ETIN
OPEN (15, FILE = ETIN)
REWIND (15)

C
C LINE 1: PRESSURE
C LINE 2: PROJECTILE TRAVEL
C LINE 3: ELECTRICAL ENERGY INPUT
C LINE 4: THERMOCHEMICAL VALUES BASED ON ELECTRICAL ENERGY INPUT
C LINE 5: INITIAL DATA
C Each file contains descriptor on line 1, number of points on line 2,
C time vs parameter on other lines or thermochems.
READ (15, 5000) PRESIN
READ (15, 5000) TRAVIN
READ (15, 5000) ELECIN
```

```

READ (15, 5000) THERIN
READ (15, 5000) INTIN
CALL OUTPUT (1)
CALL PRESS (1)
CALL TRAVEL (1)
CALL ELECTR (1)
CALL INITIAL
CALL THERM (1, IREAC)
CALL OUTPUT (2)

C
C INITIALIZE AT TIME=0.
C SET UP ARRAY FOR WF TO FIND DERIVATIVE
  TIME = 0.0
  WF2 = 0.
  WFTIM (1) = 0.0
  WFCUM (1) = 0.0
  IEND = 0
  NWF = 1
  CALL PRESS (2)
  CALL TRAVEL (2)
  CALL THERM (2, IREAC)
  CALL OUTPUT (3)

C
C TAKE FIRST TIME STEP
  TIME = TIME + TIMINC

C
C INITIAL GUESS FOR MASS OF FLUID CONSUMED IN INITIAL
C ITERATE TO MATCH THERMOCHEMS WITH MASS CONSUMED
1000 CONTINUE
  CALL PRESS (2)
  CALL TRAVEL (2)
  CALL ELECTR (2)
  M = 0

C
C IF IREAC=0, NO REACTION (EL EN DENSITY NOT LARGE ENOUGH)
C IF IREAC=1, REACTION
1010 CONTINUE
  CALL THERM (2, IREAC)
  IF (IREAC .EQ. 0) THEN
    CALL SPMEAN
    CALL OUTPUT (3)
    TIME = TIME + TIMINC
    GO TO 1000
  END IF

C
  CALL STATE

C
C M IS COUNTER--CONVERGE BEFORE 100 STEPS OR SKIP
  IF (M .GT. 100) THEN

```

```

        WRITE (*, 6010) TIME
6010  FORMAT(1X, 'TIME=' ,F10.5, ' NO CONVERGENCE')
      TIME = TIME + TIMINC
      GO TO 1000
END IF
IF ((ABS (WF1 - WF2)) .LE. TOL) THEN
C FILL ARRAY FOR WF TO FIND DERIVATIVE
  NWF = NWF + 1
  WFTIM (NWF) = TIME
  WFCUM (NWF) = WF2
  CALL OUTPUT (3)
  TIME = TIME + TIMINC
C
C END CONDITIONS
  IF (TIME .GT. TIMEND) GO TO 1020
  IF (WF2 .LE. 0.) GO TO 1020
C END IF ALL FLUID CONSUMED
  IF ((WF2 .GE. WFMASI) .AND. (IEND .EQ. 0)) THEN
    WRITE (*, *) 'All fluid consumed.'
    WRITE (*, *) 'Solution continues to balance energy.'
    IEND = 1
  END IF
C
C READY TO TAKE ANOTHER STEP
  WF1 = WF2
  GO TO 1000
ELSE
  WF1 = WF2
  M = M + 1
  GO TO 1010
END IF
C
5000 FORMAT (A20)
C
C POST PROCESSING--TAKE DERIVATIVES
1020 CONTINUE
  CALL OUTPUT (4)
  CLOSE (26, STATUS = 'KEEP')
  CLOSE (27, STATUS = 'KEEP')
  CLOSE (28, STATUS = 'KEEP')
  CLOSE (29, STATUS = 'KEEP')
  STOP
END
C ****
SUBROUTINE PRESS (IOPT)
C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /NAME/ PRESIN, TRAVIN, ELECIN, THERIN, INITIN

```

```

COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1 TRTIM (1:NPT), TRAV (1:NPT),
2 VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1 ELECEN, TEMP, RIMPET, GAMMA,
2 COVOL, WF1, WF2, ELDEN, SPPMR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
C
C CHARACTER*20 PRESIN, TRAVIN, ELECIN, THERIN, INITIN, IDENT
C
C
C IOPT=1 READ FILE
C TIME IN MS, PRESSURE IN MPa
C CHANGE TIME TO SEC
C CHANGE PRESSURE FROM MPa TO CONSISTENT UNITS WITH CGS SYSTEM
C BY MULTIPLYING BY 1.0E7 CONVERSION CONSTANT
C
IF (IOPT .EQ. 2) GO TO 1000
OPEN (21, FILE = PRESIN, STATUS = 'OLD', IOSTAT = IOS, ERR = 1010)
REWIND (21)
1010 CONTINUE
IF (IOS .NE. 0) WRITE (*, 6000) IOS
6000 FORMAT(' ERROR OPENING PRESSURE FILE:',15)
READ (21, 5000) IDENT
WRITE (*, 6010) PRESIN
C
C      WRITE(*,620) IDENT
READ (21, *) NPR
DO 1020 I = 1, NPR
      READ (21, *) PRTIM (I), PRES (I)
C CHANGE TO SEC AND CGS SYSTEM
      PRTIM (I) = PRTIM (I)*1.0E-3
      PRES (I) = PRES (I)*1.0E7
1020 CONTINUE
GO TO 1030
C
C IOPT=2 INTERPOLATE
1000 CONTINUE
      TIMTOL = ABS (TIME - .1E-10)
      IF ((TIME .EQ. 0.0) .or. (TIMTOL .EQ. 0.)) THEN
          PRESCH = PRES (1)
          CALL SPMEAN
      END IF
      DO 1040 I = 2, NPR
          IF (TIME .EQ. PRTIM (I)) PRESCH = PRES (I)
          IF (TIME .GT. PRTIM (I - 1)) THEN
              PRESCH = PRES (I - 1) + (PRES (I) - PRES (I - 1))*  

1          ((TIME - PRTIM (I - 1))/(PRTIM (I) - PRTIM (I - 1)))
      END IF

```

```

1040 CONTINUE
C
5000 FORMAT (A80)
6010 FORMAT(' Pressure-time file:',A20)
8000 FORMAT(' Pressure-time ident:',A20,/)
1030 CONTINUE
    RETURN
    END
C ****
SUBROUTINE TRAVEL (IOPT)
C
C DETERMINE PROJECTILE TRAVEL
C CALL SUBROUTINE TO DETERMINE PROJECTILE VELOCITY
    IMPLICIT REAL (A - H, O - Z)
    PARAMETER (NPT = 150, NPTT = 50)
    COMMON /NAME/ PRESIN, TRAVIN, ELECIN, THERIN, INITIN
    COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1   TRTIM (1:NPT), TRAV (1:NPT),
2   VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
    COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
    COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1   ELECEN, TEMP, RIMPET, GAMMA,
2   COVOL, WF1, WF2, ELDEN, SPMPR, VELP, BETA, BASEPR, CM,
3   Z, RHO, ENCOMP
    COMMON /OPTIONS/ IBETA, ICOM
C
CHARACTER*20 PRESIN, TRAVIN, ELECIN, THERIN, INITIN, IDENT
C
IF ((IOPT .NE. 1) .AND. (IOPT .NE. 2))
1  WRITE (*, *) ' Error in Subroutine Travel.'
C
C IOPT=1 READ FILE
C IF 2ND LINE IS 1: TIME IN MS, TRAVEL IN CM
C IF 2ND LINE IS 2: TIME IN MS, TRAVEL IS IN CM, VELOCITY IN CM/S
C CHANGE TIME TO SEC
C TRAVEL MUST BE IN CM
C VELOCITY IN CM/S
C
IF (IOPT .EQ. 2) GO TO 1000
OPEN (21, FILE = TRAVIN, STATUS = 'OLD', IOSTAT = IOS, ERR = 1010)
REWIND (21)
1010 CONTINUE
IF (IOS .NE. 0) WRITE (*, 6000) IOS
6000  FORMAT(" ERROR OPENING TRAVEL FILE:",I5)
READ (21, 5000) IDENT
WRITE (*, 6010) TRAVIN
C      WRITE(*,620) IDENT
C ITRVEL=1 FOR TIME, TRAVEL PAIRS
C ITRVEL=2 FOR TIME, TRAVEL, VELOCITY PAIRS

```

```

READ (21, *) ITRVEL
IF (ITRVEL .EQ. 1) WRITE (*, 6020)
IF (ITRVEL .EQ. 2) WRITE (*, 6030)
IF ((ITRVEL .NE. 1) .AND. (ITRVEL .NE. 2)) THEN
    WRITE (*, 6040)
    STOP
END IF
READ (21, *) NTR
DO 1020 I = 1, NTR
C
C READ TIME-TRAVEL IF ITRVEL=1
C CHANGE TIME TO SEC
C **IBHVG2
C CHANGE TRAVEL TO CM (GIVEN IN .1 MM), VEL TO CM/SEC
C     IF (ITRVEL .EQ. 1) THEN
C         READ(21,*) TRTIM(I),TRAV(I)
C         TRTIM(I)=TRTIM(I)*1.0E-3
C         TRAV(I)=TRAV(I)*0.01
C     ENDIF
C
C READ TIME-TRAVEL-VELOCITY IF ITRVEL=2
C     IF (ITRVEL .EQ. 2) THEN
C         READ(21,*) TRTIM(I),TRAV(I),VEL(I)
C         TRTIM(I)=TRTIM(I)*1.0E-3
C         TRAV(I)=TRAV(I)*0.01
C         VEL(I)=VEL(I)*0.1
C     ENDIF
C ***
C TIME IN MS, TRAVEL GIVEN IN CM
    IF (ITRVEL .EQ. 1) THEN
        READ (21, *) TRTIM (I), TRAV (I)
        TRTIM (I) = TRTIM (I)*1.0E-3
    END IF
C
1020 CONTINUE
GO TO 1030
C
C IOPT=2 INTERPOLATE
1000 CONTINUE
    IF (TIME .EQ. 0.) THEN
        TRAVPR = TRAV (1)
        VELP = 0.0
    END IF
C
C ITRVEL=1 HAVE JUST TIME-TRAVEL
    IF (ITRVEL .EQ. 1) THEN
        DO 1040 I = 2, NTR
            IF (TIME .EQ. TRTIM (I)) THEN
                TRAVPR = TRAV (I)

```

```

        CALL VELPR (I)
        GO TO 1030
    END IF
    IF (TIME .GT. TRTIM (I - 1)) THEN
        TRAVPR = TRAV (I - 1) + (TRAV (I) - TRAV (I - 1))*  

1           ((TIME - TRTIM (I - 1))/(TRTIM (I) - TRTIM (I - 1)))
        CALL VELPR (I)
    END IF
1040   CONTINUE
    END IF
C
C ITRVEL=2 HAVE TIME-TRAVEL-VELOCITY
    IF (ITRVEL .EQ. 2) THEN
        DO 1050 I = 2, NTR
            IF (TIME .EQ. TRTIM (I)) THEN
                TRAVPR = TRAV (I)
                VELP = VEL (I)
                GO TO 1030
            END IF
            IF (TIME .GT. TRTIM (I - 1)) THEN
                TRAVPR = TRAV (I - 1) + (TRAV (I) - TRAV (I - 1))*  

1                   ((TIME - TRTIM (I - 1))/(TRTIM (I) - TRTIM (I - 1)))
                VELP = VEL (I - 1) + (VEL (I) - VEL (I - 1))*  

1                   ((TIME - TRTIM (I - 1))/(TRTIM (I) - TRTIM (I - 1)))
            END IF
1050   CONTINUE
    END IF
C
5000 FORMAT (A80)
6010 FORMAT(' Proj motion-time file:',A20)
8000 FORMAT(' Proj motion-time ident:',A20,/)
6020 FORMAT(' Proj travel-time file.',/)
6030 FORMAT(' Proj velocity-time file.',/)
6040 FORMAT(' Error--unknown type file.',/)
1030 CONTINUE
    RETURN
END
C ****
SUBROUTINE ELECTR (IOPT)
C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /NAME/ PRESIN, TRAVIN, ELECIN, THERIN, INTIN
COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1  TRTIM (1:NPT), TRAV (1:NPT),
2  VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1  ELECEN, TEMP, RIMPET, GAMMA,

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2 COVOL, WF1, WF2, ELDEN, SPPMR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
C
CHARACTER*20 PRESIN, TRAVIN, ELECIN, THERIN, INITIN, IDENT
C
IF ((IOPT .NE. 1) .AND. (IOPT .NE. 2))
1 WRITE (*, *) ' Error in Subroutine Electr.'
C
C IOPT=1 READ FILE
C ELECTRICAL ENERGY IS CUMULATIVE
C TIME IN MS, ELECTRICAL ENERGY IN kJ
C CHANGE TIME TO SEC
C
IF (IOPT .EQ. 2) GO TO 1000
OPEN (21, FILE = ELECIN, STATUS = 'OLD', IOSTAT = IOS, ERR = 1010)
REWIND (21)
1010 CONTINUE
IF (IOS .NE. 0) WRITE (*, 6000) IOS
6000 FORMAT(' ERROR OPENING ELECTRICAL ENERGY FILE:',I5)
READ (21, 5000) IDENT
WRITE (*, 6010) ELECIN
C
      WRITE(*,620) IDENT
READ (21, *) NEL
DO 1020 I = 1, NEL
  READ (21, *) ELTIM (I), ELEC (I)
  ELTIM (I) = ELTIM (I)*1.0E-3
1020 CONTINUE
GO TO 1030
C
C IOPT=2 INTERPOLATE
1000 CONTINUE
IF (TIME .EQ. 0.) ELECEN = ELEC (1)
DO 1040 I = 2, NEL
  IF (TIME .EQ. ELTIM (I)) ELECEN = ELEC (I)
  IF (TIME .GT. ELTIM (I - 1)) THEN
    ELECEN = ELEC (I - 1) + (ELEC (I) - ELEC (I - 1))*(
1      ((TIME - ELTIM (I - 1))/(ELTIM (I) - ELTIM (I - 1))))
  END IF
1040 CONTINUE
C
5000 FORMAT (A80)
6010 FORMAT(' Electrical energy-time file:',A20)
8000 FORMAT(' Electrical energy-time ident:',A20/)
1030 CONTINUE
RETURN
END
C ****
SUBROUTINE INITIAL

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C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /NAME/ PRESIN, TRAVIN, ELECIN, THERIN, INITIN
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
1 PROJI, PROJW, TOL, TIMINC,
2 TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1 ELECEN, TEMP, RIMPET, GAMMA,
2 COVOL, WF1, WF2, ELDEN, SPMPR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM

C
CHARACTER*20 PRESIN, TRAVIN, ELECIN, THERIN, INITIN, IDENT

C
OPEN (21, FILE = INITIN, STATUS = 'OLD', IOSTAT = IOS, ERR = 1000)
REWIND (21)
1000 CONTINUE
IF (IOS .NE. 0) WRITE (*, 6000) IOS
6000 FORMAT(' ERROR OPENING INITIAL DATA FILE:', I5)

C
C CHAMBER VOLUME IN CM^3
C INITIAL PROJECTILE POSITION IN CM WITH 0.0 AT ORIGIN OF TUBE
C TUBE DIAMETER IN CM--AREA IN CM^2
C PROJECTILE MASS IN KG
C INITIAL MASS OF WORKING FLUID IN GRAMS
C DENSITY OF WORKING FLUID IN G/CM^3
C TIME INCREMENT IN SEC
READ (21, 5000) IDENT
WRITE (*, 6010) INITIN
C   WRITE(*,620) IDENT
READ (21, *) CHVOL
WRITE (*, 6020) CHVOL
C TUBE DIAMETER
READ (21, *) DIAM
AREA = 3.141592654*(DIAM/2.)*(DIAM/2.)
WRITE (*, 6030) DIAM, AREA
C PROJECTILE INITIAL POSITION AND MASS (CHANGE KG TO G)
READ (21, *) PROJI
IF (PROJI .NE. 0.0) WRITE (*, *)
1  ' Change needed--proj not zeroed.'
READ (21, *) PROJW
WRITE (*, 6040) PROJI, PROJW
PROJW = PROJW*1000.
C WORKING FLUID INITIAL MASS
READ (21, *) WFMASI
WRITE (*, 6050) WFMASI
READ (21, *) RHOI
WRITE (*, 6060) RHOI

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RHO = RHOI
C TOLERANCE IN ITERATION
  READ (21, *) TOL
  WRITE (*, 6070) TOL
C TIME IN SEC
  READ (21, *) TIME
  READ (21, *) TIMINC
  READ (21, *) TIMEND
  WRITE (*, 6080) TIME, TIMINC, TIMEND
C INITIAL GUESS FOR MASS OF WORKING FLUID CONSUMED
  READ (21, *) WF1
  WRITE (*, 6090) WF1
C READ INITIAL VALUE OF BETA
C OPTIONS FOR BETA:
C   BETA IS INITIAL VALUE OF WORKING FLUID MOVING--
C   LAGRANGE ASSUMPTION IS BETA=1, I.E. ALL FLUID MOVES
C   IF BETA=0., FLUID IS AT REST
C   CHANGE FRACTION OF BETA MOVING IF IBETA=1
C   IF IBETA=0, LET BETA=CONSTANT (INITIAL VALUE)
C   IF IBETA=1, LET BETA=Z (FRACTION OF WF REACTED)
  READ (21, *) BETA, IBETA
  WRITE (*, 6100) BETA
  IF (IBETA .EQ. 1) THEN
    WRITE (*, 6110) IBETA
    Z = 0.
  END IF
C MASS OF AIR INITIALLY IN CHAMBER
  READ (21, *) WAIR
  WRITE (*, 6120) WAIR
C
C OPTION - COMPRESSION OF WORKING FLUID
C IF ICOM=0, DO NOT CONSIDER COMPRESSION
C IF ICÓM=1, CONSIDER COMPRESSION
  READ (21, *) ICOM
  IF ((ICOM .NE. 0) .AND. (ICOM .NE. 1)) WRITE (*, *) 'Error--ICOM'
C BM=BULK MODULUS OF FLUID AT ONE ATMOSPHERE (MPa)
C DERBM=DERIVATIVE OF BULK MODULUS WITH RESPECT TO PRESSURE
  IF (ICOM .EQ. 1) THEN
    READ (21, *) BM, DERBM
    WRITE (*, 6130) BM, DERBM
C CHANGE TO CGS
  BM = BM*1.0E7
  END IF
C
  5000 FORMAT (A80)
  6010 FORMAT(' Initial data file:',A20)
  8000 FORMAT(' Initial data ident:',A20)
  6020 FORMAT(' Chamber volume (cm^3)=',F15.5)
  6030 FORMAT(' Tube diameter (cm)=',F6.1,2x,' Area (cm^2)=',F12.5)

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6040 FORMAT(' Projectile position (cm)=',F10.5,
     1           2X,' Projectile mass (kg)=',F10.2)
6050 FORMAT(' Working fluid mass (g)=',F10.5)
6060 FORMAT(' Initial working fluid density (g/cm^3)=',F10.5)
6070 FORMAT(' Tolerance required in mass consumed=',F10.5)
6080 FORMAT(' Time start (sec)=',F10.8,' Time increment (sec)=',
     1           F10.8,' Time end (sec)=',F10.8)
6090 FORMAT(' Initial guess for mass consumed (g)=',F10.5)
6100 FORMAT(' Initial value of beta, fraction of wf moving (-)=',F10.5)
6110 FORMAT(' Option: ibeta=',I5,/,
     1' If ibeta=0 fraction moving is constant',/
     2' If ibeta=1, fraction moving=fraction decomposed')
6120 FORMAT(' Mass of air initially in chamber (g)=',F10.5)
6130 FORMAT(' Bulk modulus of WF at one atmosphere (MPa)=',F10.5,/)
     1' Derivative of bulk modulus wrt pressure (-)=',F10.5,/)
C
CLOSE (21)
RETURN
END
C ****
SUBROUTINE THERM (IOPT, IREAC)
C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /NAME/ PRESIN, TRAVIN, ELECIN, THERIN, INITIN
COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
1 PROJ, PROJW, TOL, TIMINC,
2 TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1 ELECEN, TEMP, RIMPET, GAMMA,
2 COVOL, WF1, WF2, ELDEN, SPMMPR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
COMMON /THERMO/ ELDEN1 (1:NPTT), TEMP1 (1:NPTT), RIMP1 (1:NPTT),
1 GAMMA1 (1:NPTT), COVOL1 (1:NPTT)
C
CHARACTER*20 PRESIN, TRAVIN, ELECIN, THERIN, INITIN, IDENT
C
IF ((IOPT .NE. 1) .AND. (IOPT .NE. 2))
1 WRITE (*, *) ' Error in Subroutine Electr.'
C
C IOPT=1 READ FILE
IF (IOPT .EQ. 2) GO TO 1000
C BASED ON AMOUNT OF ELECTRICAL ENERGY INPUT
OPEN (21, FILE = THERIN, STATUS = 'OLD', IOSTAT = IOS, ERR = 1010)
REWIND (21)
1010 CONTINUE
IF (IOS .NE. 0) WRITE (*, 6000) IOS

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6000 FORMAT(' ERROR OPENING THERMOCHEM DATA FILE:',I5)
C
C ELECTRICAL ENERGY DENSITY (Elec en/mass fluid in chamber) IN kJ/G
C TEMPERATURE IN K
C IMPETUS IN J/G
C GAMMA, RATIO OF SPECIFIC HEAT, UNITLESS
C COVOLUME IN CM^3/G
C CONVERT JOULES TO CGS: 1 JOULE=1.0E7 G-CM^2/S^2
    READ (21, 5000) IDENT
    WRITE (*, 6010) THERIN
C    WRITE(*,620) IDENT
    READ (21, *) NTH
    DO 1020 I = 1, NTH
        READ (21, *) ELDEN1 (I), TEMP1 (I), RIMP1 (I),
        1      GAMMA1 (I), COVOL1 (I)
C ELECTRICAL ENERGY DENSITY IN kJ/G
        RIMP1 (I) = RIMP1 (I)*1.0E+7
1020 CONTINUE
    GO TO 1030
C
1000 CONTINUE
C ELECTRICAL ENERGY DENSITY=CUMULATIVE ELEC ENERGY/CUMULATIVE WF REACTED
    IF (WF1 .LT. 0.0) THEN
        WRITE (*, 6020)
    END IF
C ASSUME FIRST LINE OF TABLE IS 0.
    IF ((WF1 .LE. 0.) .OR. (TIME .EQ. 0.)) THEN
        TEMP = TEMP1 (1)
        RIMPET = RIMP1 (1)
        GAMMA = GAMMA1 (1)
        COVOL = COVOL1 (1)
        GO TO 1030
    END IF
C
    IF (WF1 .GT. 0.) ELDEN = ELECEN/WF1
C
C IF WF CONSUMED, FIX THERMOCHEMS AT FINAL VALUE
    IF (WF1 .GT. WFMASI) ELDEN = ELECEN/WFMASI
C
C IF EL EN DENSITY NOT LARGE ENOUGH FOR REACTION,
C COMMUNICATE TO MAIN WITH IREAC=0 AND SKIP THIS STEP
    IF (ELDEN .LT. ELDEN1 (1)) THEN
        IREAC = 0
        GO TO 1030
    END IF
C
    DO 1040 I = 2, NTH
        IF (ELDEN .EQ. ELDEN1 (I)) THEN
            TEMP = TEMP1 (I)

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RIMPET = RIMP1 (I)
GAMMA = GAMMA1 (I)
COVOL = COVOL1 (I)
END IF
IF (ELDEN .GT. ELDEN1 (I - 1)) THEN
    TEMP = TEMP1 (I - 1) + (TEMP1 (I) - TEMP1 (I - 1))*  

    1   ((ELDEN - ELDEN1 (I - 1))/(ELDEN1 (I) - ELDEN1 (I - 1)))
    RIMPET = RIMP1 (I - 1) + (RIMP1 (I) - RIMP1 (I - 1))*  

    1   ((ELDEN - ELDEN1 (I - 1))/(ELDEN1 (I) - ELDEN1 (I - 1)))
    GAMMA = GAMMA1 (I - 1) + (GAMMA1 (I) - GAMMA1 (I - 1))*  

    1   ((ELDEN - ELDEN1 (I - 1))/(ELDEN1 (I) - ELDEN1 (I - 1)))
    COVOL = COVOL1 (I - 1) + (COVOL1 (I) - COVOL1 (I - 1))*  

    1   ((ELDEN - ELDEN1 (I - 1))/(ELDEN1 (I) - ELDEN1 (I - 1)))
END IF
IREAC = 1
1040 CONTINUE
C
C IF FALL OUTSIDE ARRAY
IF (ELDEN .GT. ELDEN1 (NTH)) THEN
    TEMP = TEMP1 (NTH)
    RIMPET = RIMP1 (NTH)
    GAMMA = GAMMA1 (NTH)
    COVOL = COVOL1 (NTH)
    WRITE (26, *) ' OUTSIDE THERM ARRAY'
END IF
C
5000 FORMAT (A80)
6010 FORMAT(' Thermochemical data file:',A20)
8000 FORMAT(' Thermochemical data ident:',A20,/)
6020 FORMAT(' Error in Subroutine Electr--El En Density negative.')
C
1030 CONTINUE
RETURN
END
C *****
SUBROUTINE STATE
C
IMPLICIT REAL (A - H, O - Z)
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
1 PROJI, PROJW, TOL, TIMINC,
2 TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1 ELECEN, TEMP, RIMPET, GAMMA,
2 COVOL, WF1, WF2, ELDEN, SPMMPR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
C
C DETERMINE SPACE-MEAN PRESSURE
CALL SPMEAN

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C
C IF ICOM=0, DO NOT CONSIDER COMPRESSION OF WF
C IF ICOM=1, CONSIDER COMPRESSION OF WF
C   ENCOMP IS ENERGY PER UNIT MASS STORED BY COMPRESSED FLUID
C     --NEED TO MULTIPLY BY AMT OF FLUID UNVAPORIZED
  IF (ICOM .EQ. 0) THEN
    RHO = RHOI
    ENCOMP = 0.0
  END IF
  IF (ICOM .EQ. 1) CALL COMPRES
C
C CUMULATIVE FLUID CONSUMED FROM ENERGY EQN, P 105, BK 9
  GAM1 = GAMMA - 1.
  DIV = RIMPET/GAM1 + SPMPR*(COVOL/GAM1 - 1./(RHO*GAM1))
C
  TOP = (CHVOL - WFMASI/RHO + TRAVPR*AREA)*(SPMPG/GAM1)
  1  + VELP*VELP*((1./6.)*CM*PROJW + .5*PROJW)
  2  + (1. - Z)*WFMASI*ENCOMP
C
  Z = (1./WFMASI)*(TOP/DIV)
  WF2 = Z*WFMASI
C
  RETURN
END
C *****
SUBROUTINE SPMEAN
C
IMPLICIT REAL (A - H, O - Z)
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
  1 PROJI, PROJW, TOL, TIMINC,
  2 TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
  1 ELECEN, TEMP, RIMPET, GAMMA,
  2 COVOL, WF1, WF2, ELDEN, SPMPR, VELP, BETA, BASEPR, CM,
  3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
C
C SPACE MEAN PRESSURE EQUALS CHAMBER PRESSURE (IF EXPERIMENTAL)
C   SPMPR=PRESCH
C
C SPACE-MEAN PRESSURE FROM LAGRANGE GRADIENT
C ASSUME PRESCH IS A PRESSURE MEASUREMENT AT THE BREECH
C INCREASE PROJECTILE MASS BY 5% TO ACCOUNT FOR FRICTION
C CHARGE TO MASS RATIO, CM, IS INITIAL MASS OF WORKING FLUID
C DIVIDED BY MASS OF PROJECTILE
C   projw=1.05*PROJW
C For test case, no friction
  ALPHA = WF2/WFMASI
C

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C CONSIDER BETA=FRACTION OF FLUID WHICH MOVES
C IF BETA=0., ALL THE FLUID IS AT REST
C IF BETA=1., ALL THE WF MOVES (LAGRANGE ASSUMP)
  IF (IBETA .EQ. 1) BETA = Z
  CM = (WFMASI*(ALPHA + BETA*(1. - ALPHA)) + WAIR)/PROJW
  IF (CM .LE. 0.0) WRITE (*, *) ' Error in Spmean--C/M <= 0.'
  SPMPR = ((1. + 1./3.*CM)/(1. + 1./2.*CM))*PRESCH
  BASEPR = (1. / (1. + 1./3.*CM))*SPMPR
C
  RETURN
  END
C *****
C SUBROUTINE COMPRES
C
C DETERMINE DENSITY OF COMPRESSED WORKING FLUID
C DETERMINE ENERGY OF COMPRESSION
C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
1 PROJ, PROJW, TOL, TIMINC,
2 TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1 ELECEN, TEMP, RIMPET, GAMMA,
2 COVOL, WF1, WF2, ELDEN, SPMPR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1 TRTIM (1:NPT), TRAV (1:NPT),
2 VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
C
C LET BULK MODULUS BE AT MOST A LINEAR FCN OF PRESSURE
  IF (BM .LE. 0.0) WRITE (*, *) 'ERROR--BM<=0.0'
  IF (DERBM .EQ. 0.0) THEN
    RHO = RHOI*(1. + (PRESCH - PRES (1))/BM)
  ELSE
    RHO = RHOI*(1. + (DERBM/BM)*(PRESCH - PRES (1)))**(1./DERBM)
  END IF
C
C ENERGY PER UNIT MASS STORED BY COMPRESSED FLUID
  IF ((DERBM .EQ. 0.0) .OR. (DERBM .EQ. 1.0)) THEN
    ENCOMP = - 1. *(PRESCH - PRES (1))/RHO + (BM/RHO)*
1 LOG (1. + (PRESCH - PRES (1))/BM)
  ELSE
    ENCOMP = - 1. *(PRESCH - PRES (1))/RHO + (BM +
1 DERBM*(PRESCH - PRES (1)))
2 /((DERBM - 1.)*RHO) - BM/((DERBM - 1.)*RHO)
  END IF
C

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RETURN
END
C *****
SUBROUTINE VELPR (I)
C
C DETERMINE PROJECTILE VELOCITY
C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1 TRTIM (1:NPT), TRAV (1:NPT),
2 VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
1 PROJI, PROJW, TOL, TIMINC,
2 TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1 ELECEN, TEMP, RIMPET, GAMMA,
2 COVOL, WF1, WF2, ELDEN, SPPMR, VELP, BETA, BASEPR, CM,
3 Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
C
C CENTERED DIFFERENCE
IF (I .EQ. NTR) THEN
  VELP = (TRAV (I) - TRAV (I - 2))/(2.*  

1   (TRTIM (I) - TRTIM (I - 1)))
ELSE
  VELP = (TRAV (I + 1) - TRAV (I - 1))/(2.*  

1   (TRTIM (I) - TRTIM (I - 1)))
END IF
C
RETURN
END
C *****
SUBROUTINE DER (TIME, IOPT, AMT, AMTDER)
C
C FINDS DERIVATIVES: USED FOR dE/dt and dWF/dt
C ASSUMES CONSTANT STEP SIZE FOR TIME
C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1 TRTIM (1:NPT), TRAV (1:NPT),
2 VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
COMMON /OUT/ WFTIM (NPT), WFCUM (NPT)
COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
C
C IF IOPT=1, FIND DER OF ENERGY
C IF IOPT=2, FIND DER OF WF

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IF (IOPT .EQ. 1) GO TO 1000
IF (IOPT .EQ. 2) GO TO 1010
C
IF ((ABS (TIME - 1.E-10)) .EQ. 0.0) THEN
  AMT = 0.0
  AMTDER = 0.0
  GO TO 1020
END IF
C
C IOPT=1, DERIVATIVE OF ELEC EN
1000 CONTINUE
DO 1030 I = 2, NEL
  IF (TIME .EQ. ELTIM (I)) THEN
    AMT = ELEC (I)
    IMARK = I
    GO TO 1040
  END IF
  IF (TIME .GT. ELTIM (I - 1)) THEN
    AMT = ELEC (I - 1) + (ELEC (I) - ELEC (I - 1))*  

    1   ((TIME - ELTIM (I - 1))/(ELTIM (I) - ELTIM (I - 1)))
    IMARK = I
  END IF
1030 CONTINUE
C IF GREATER THAN LAST POINT, USE LAST POINT
C CENTERED DIFFERENCE
1040 CONTINUE
  IF (IMARK .EQ. NEL) THEN
    AMT = ELEC (NEL)
    AMTDER = (ELEC (IMARK) - ELEC (IMARK - 2))/(2.*(ELTIM (IMARK)  

    1   - ELTIM (IMARK - 1)))
  ELSE
    AMTDER = (ELEC (IMARK + 1) - ELEC (IMARK -  

    1   1))/(2.*(ELTIM (IMARK  

    2   - ELTIM (IMARK - 1)))
  END IF
C
  GO TO 1020
C
C IOPT=2 DERIVATIVE OF WF
1010 CONTINUE
C
DO 1050 I = 2, NWF
  IF (TIME .EQ. WFTIM (I)) THEN
    AMT = WFCUM (I)
    IMARK = I
    GO TO 1060
  END IF
  IF (TIME .GT. WFTIM (I - 1)) THEN
    AMT = WFCUM (I - 1) + (WFCUM (I) - WFCUM (I - 1))*  


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1      ((TIME - WFTIM (I - 1))/(WFTIM (I) - WFTIM (I - 1)))
IMARK = I
END IF
1050 CONTINUE
C IF GREATER THAN LAST POINT, USE LAST POINT
C CENTERED DIFFERENCE
1060 CONTINUE
IF (IMARK .EQ. NWF) THEN
  AMT = WFCUM (NWF)
  AMTDER = (WFCUM (IMARK) - WFCUM (IMARK - 2))/(2.*(WFTIM (IMARK)
1      - WFTIM (IMARK - 1)))
ELSE
  AMTDER = (WFCUM (IMARK + 1) - WFCUM (IMARK -
1      1))/(2.*(WFTIM (IMARK)
2      - WFTIM (IMARK - 1)))
END IF
C
1020 CONTINUE
RETURN
END
C ****
SUBROUTINE OUTPUT (IOPT)
C
IMPLICIT REAL (A - H, O - Z)
PARAMETER (NPT = 150, NPTT = 50)
COMMON /START/ CHVOL, AREA, WFMASI, RHOI,
1  PROJI, PROJW, TOL, TIMINC,
2  TIMEND, WAIR, BM, DERBM
COMMON /CURRENT/ TIME, PRESCH, TRAVPR,
1  ELECEN, TEMP, RIMPET, GAMMA,
2  COVOL, WF1, WF2, ELDEN, SPMMPR, VELP, BETA, BASEPR, CM,
3  Z, RHO, ENCOMP
COMMON /OPTIONS/ IBETA, ICOM
COMMON /DATA/ PRTIM (1:NPT), PRES (1:NPT),
1  TRTIM (1:NPT), TRAV (1:NPT),
2  VEL (1:NPT), ELTIM (1:NPT), ELEC (1:NPT)
COMMON /OUT/ WFTIM (NPT), WFCUM (NPT)
COMMON /NUMBER/ NPR, NTR, NEL, NTH, ITRVEL, NWF
COMMON /NAME/ PRESIN, TRAVIN, ELECIN, THERIN, INITIN
CHARACTER*20 PRESIN, TRAVIN, ELECIN, THERIN, INITIN
C
C FILE 28 IS OUTPUT FOR DETAILS OF WORKING FLUID
C FILE 27 IS ENERGY BALANCE
C FILE 26 IS ERROR FILE AND MESSAGES
IF (IOPT .EQ. 1) THEN
  WRITE (*, 6000)
  OPEN (26, FILE = 'MESSAGES.OUT')
  OPEN (27, FILE = 'ENERGY.OUT')
  OPEN (28, FILE = 'WORKFL.OUT')

```

```

OPEN (29, FILE = 'COMPRESS.OUT')
GO TO 1000
END IF
IF (IOPT .EQ. 2) GO TO 1010
IF (IOPT .EQ. 3) GO TO 1020
IF (IOPT .EQ. 4) GO TO 1030
C
1010 CONTINUE
  WRITE (*, 6010)
  WRITE (*, 6020)
  WRITE (27, 6030)
  WRITE (28, 6040)
  WRITE (29, 6050)
  GO TO 1000
C
1020 CONTINUE
C CHANGE TO MPa AND TO JOULES
  TIMMS = TIME*1.0E+3
  PRESCH = PRESCH*1.0E-7
  BASEPR = BASEPR*1.0E-7
  SPMMPR = SPMMPR*1.0E-7
  WRITE (*, 6060) TIMMS, PRESCH, BASEPR, TRAVPR, VELP, ELDEN, WF2
  write (26, 6070) timms, presch, basepr
  rimpel = rimpel*1.0e-7
  enused = (rimpel/(gamma - 1.))*wf2
  enkp = .5*projw*velp*velp*1.0e-7
  alpha = wf2/wfmasi
  cm = (wfmasi*(alpha + beta*(1. - alpha)) + wair)/projw
  enkg = (1./6.)*cm*projw*velp*velp*1.0e-7
  vol = chvol - covol*wf2 - (wfmasi - wf2)/rho + travpr*area
  enigas = spmmpr*vol/(gamma - 1.)
  encom = (1. - z)*wfmasi*encomp*1.0e-7
  if (enused .ne. 0.0)
    1  ener = ((enused - enkp - enkg - enigas - encom)/enused)*100.
    write (27, 6080) timms, enused, enkp, enkg, enigas, encom, ener
    write (29, 6090) timms, rho, encomp, encom
C
  GO TO 1000
C
C IF IOPT=1, FIND DER OF ENERGY
C IF IOPT=2, FIND DER OF WF
1030 CONTINUE
  TIME = 0.0
  TIMEND = WFTIM (NWF)
  TIM2 = 0.0
  EL = 0.0
  WF = 0.0
  ELDEN = 0.0
  ELDER = 0.0

```

```

WFDER = 0.0
WRITE (28, 6100) TIM2, EL, WF, ELDEN, ELDER, WFDER
DO 1040 I = 1, NPT
    TIME = TIME + TIMINC
    IF (TIME .LE. TIMEND) THEN
        CALL DER (TIME, 1, EL, ELDER)
        CALL DER (TIME, 2, WF, WFDER)
        IF (WF .NE. 0.0) ELDEN = EL/WF
        TIM2 = TIME*1.E+3
C ELDEN IN MJ/s, WFDER IN kg/s
        ELDEN = ELDEN*.001
        WFDER = WFDER*.001
        WRITE (28, 6100) TIM2, EL, WF, ELDEN, ELDER, WFDER
    ELSE
        GO TO 1000
    END IF
1040 CONTINUE
C
6000 FORMAT(/, ' Inverse Electrothermal Gun Code'//)
6010 FORMAT(1X, ' TIME ',2X,'CHAM PR',2X,
    1      ' BASE PR ',3X,'PROJ TRAV',2X,' PROJ VEL',5X,'EL EN DEN',
    2      2X,'CUM WF')
6020 FORMAT(2X, ' (ms) ',2x,2x,'(MPa)',3x,2x,1x,'(MPa)',1x,2x,
    1      2x,'(cm)',3x,2x,3x,'(cm/s)',2x,2x,2x,'(MJ/kg)',1X,
    2      2X,1X,'(g)'),/
6060 FORMAT(1X,F6.2,2X,F7.2,2X,F10.5,2X,F9.4,2X,F10.2,2X,F9.3,2X,F10.5)
6070 format(1x,f6.2,2x,f15.7,2x,f15.7)
6030 format(1x,'ENERGY BALANCE'//,
    1      1x,'time',7x,'enused',10x,'KE proj',9x,'KE gas',8x,
    2      'Intgas',5x,'En comp',5x,'Error %',
    3      /,1x,'(ms)',7x,' (J) ',11x,' (J) ',9x,' (J) ',10x,' (J) ',
    4      10x,' (J)')
6080 format(1x,f10.3,1x,f15.2,1x,f10.2,1x,f10.2,1x,f12.2,1X,F10.2,1x,
    1      F6.1)
6040 FORMAT(1x,'WORKING FLUID AND ELECTRICAL ENERGY SUMMARY'//,
    1      1x,1x,'TIME',1x,3x,'EL EN',2x,5x,'WF CUMULATIVE',1X,1x,
    2      'EL EN DENSITY',1x,'ELEC DER',1X,2x,'WF DER',
    3      /,1x,1X,'(ms)',1X,3x,'(kJ)',3X,11X,'(G)',6x,4X,'(MJ/kg)',5X,
    4      2x,'(MJ/s)',2X,3x,'(kg/s)')
6100 FORMAT(1x,f6.3,1x,f10.2,1x,f15.5,1x,f15.5,1x,f10.2,1x,f10.2)
6050 FORMAT(1x,'timms(ms),rho(g/cc),encomp(J/g),encom(J)')
6090 FORMAT(1x,f6.3,1x,f8.5,1x,f20.5,1x,f10.5)
C
1000 CONTINUE
RETURN
END
C ****

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